

Renewable Integration in Indiana Based on History

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We have many years of renewable experience

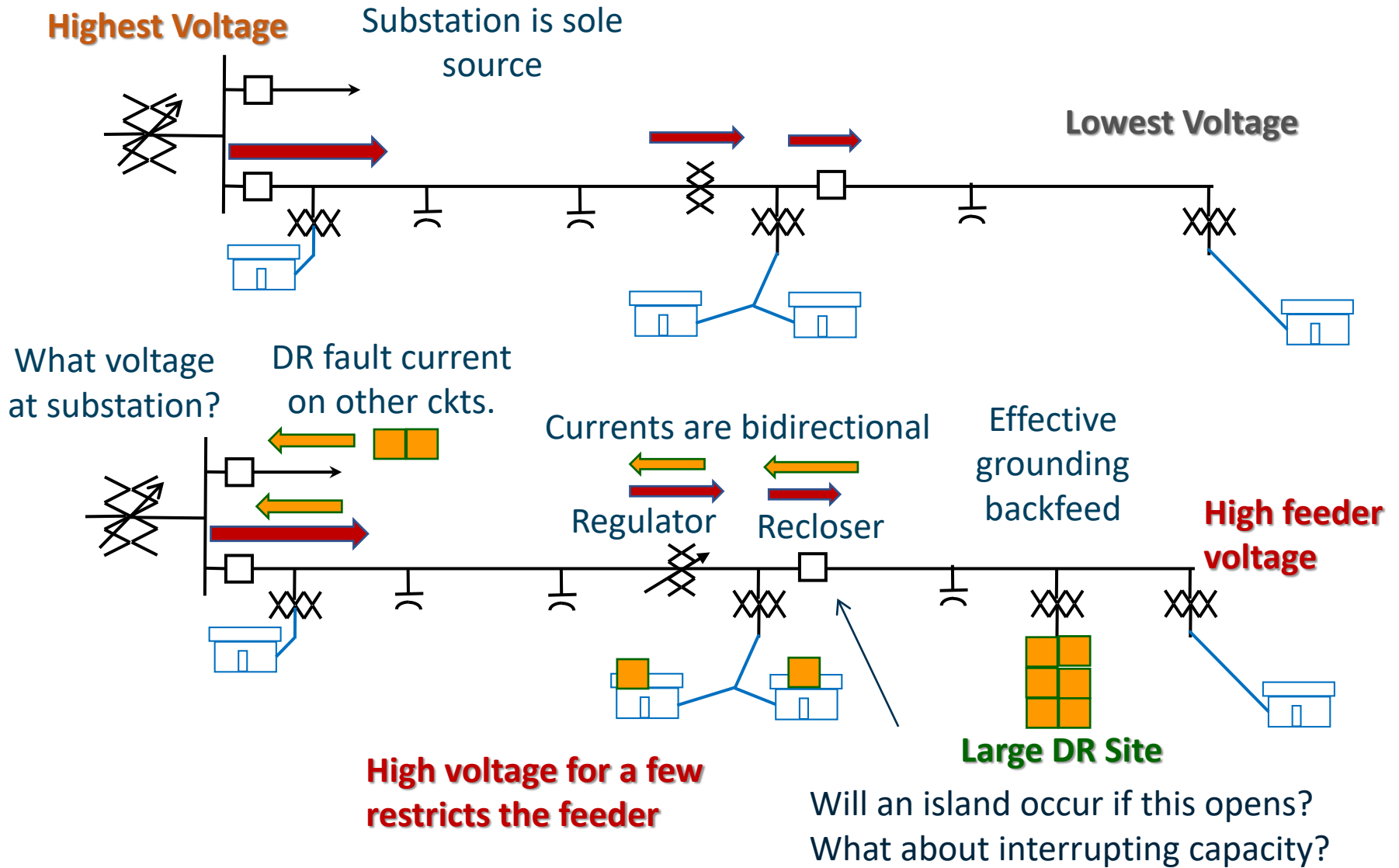
- Indianapolis was *#2 in the nation in 2014* according to the “Shining Cities” 2015 report

Table ES-2: The “Solar Stars” (Cities with 50 or More Watts of Solar PV per Person, End of 2014)

City	State	Total Solar PV Installed (MW-DC)	Total Solar PV Rank	Per Capita Solar PV Installed (Watts-DC/Person)	Per Capita Rank
Honolulu	HI	96	6	276	1
Indianapolis	IN	107	4	127	2
San Jose	CA	105	5	110	3
San Diego	CA	149	2	110	4
Wilmington	DE	7	28	101	5

- All on distribution, most is utility scale
- Also have many years of hourly wind data from MISO

Distribution is much more complicated



Distribution is much more complicated

- High/low voltage concerns – tuning inverters will help
- Less certainty about peak load potential and future risks – more need for multi-year 8,760 hourly analysis
- Effective grounding concerns – what is best way?
- Higher short circuit currents may exceed interrupting rating
- Mutual coupling models on distribution
- Conservation Voltage Reduction verification is more difficult
- Smart inverter settings – coordinate local needs with MISO
- New rules allowing aggregation on distribution
- How to figure out value of DR to distribution
- Prospect for marginal pricing
- What to do when feeder is “sold out”

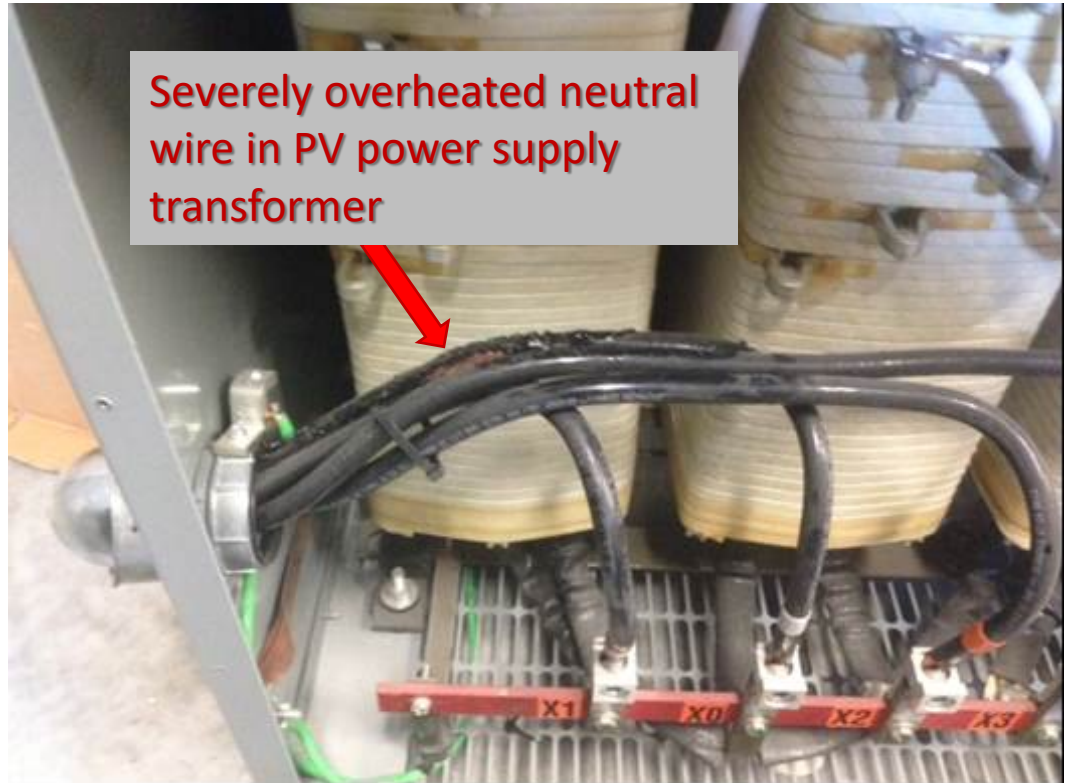
Three DG grounding options – there is no simple answer

- Ungrounded
 - Transient overvoltages at load rejection
 - No ground current back feed
 - Risk that phase to ground voltages become unstable
- Minimum effectively grounded
 - Now preferred by IPL and possibly IEEE 1547.8
 - Lower transient voltages
 - Some back feed current even when DG is not producing
 - Potential for overload of grounding equipment
- Strong effective grounding
 - Transient voltage fully controlled
 - Difficult coordinating protective devices and risk of false tripping
 - Short circuit current exceeds equipment rating
 - Highest risk of back feed even when no DG output

Note: IURC level 2 rules require acceptance if effectively grounded

Neutral overload and suspected back feed from effective grounding

- Two phases open on one 13 kV circuit
- One phase open on second 13 kV circuit with third phase in the clear
- Solar grounding likely back feed into other customers and possibly energized downed conductors in public area
- Neutral needs to be three times bigger than phase conductor
- Effective grounding needs to shut off in these situations

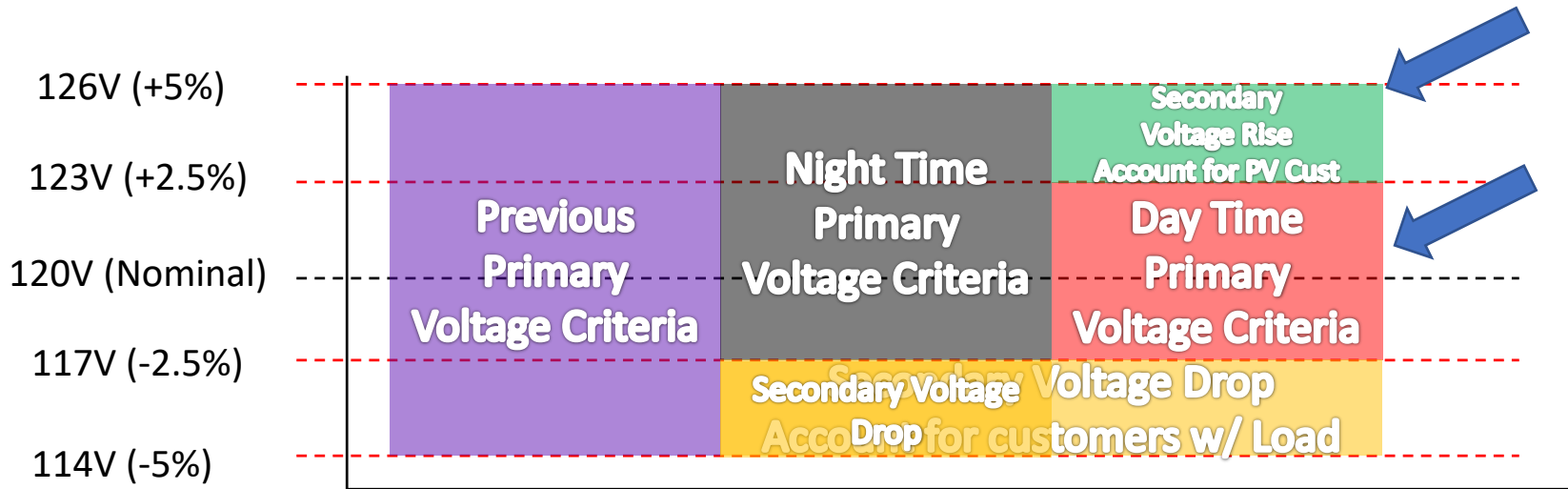


Some hosting capacity criteria we considered in California – When to accept without detailed study

Now commercial software will calculate

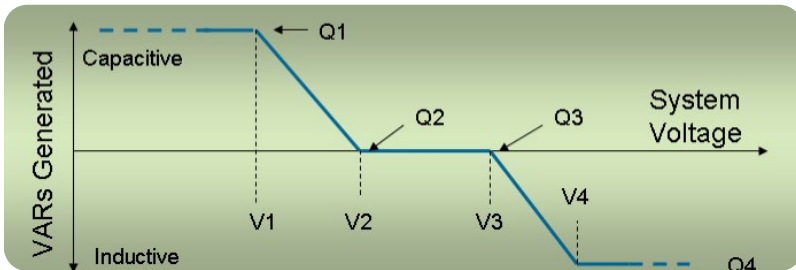
Category	Criteria	Basis	Flag
Voltage	Overvoltage	Feeder voltage	≥ 1.05 Vpu
	Voltage Deviation	Deviation in voltage from no PV to full PV	$\geq 3\%$ at primary $\geq 5\%$ at secondary $\geq \frac{1}{2}$ band at regulators
	Unbalance	Phase voltage deviation from average	$\geq 3\%$
Loading	Thermal	Element loading	$\geq 100\%$ normal rating
Protection	Total Fault Contribution	Total fault current contribution at each sectionalizing device	$\geq 10\%$ increase
	Forward Flow Fault Contribution	Forward flow fault current contribution at each sectionalizing device	$\geq 10\%$ increase
	Sympathetic Breaker Tripping	Breaker zero sequence current due to an upstream fault	$\geq 150\text{A}$
	Breaker Reduction of Reach	Deviation in breaker fault current for feeder faults	$\geq 10\%$ decrease
	Breaker/Fuse Coordination	Fault current increase at fuse relative to breaker current increase	$\geq 100\text{A}$ increase
	Anti-Islanding	PV beyond each sectionalizing device	$\geq 50\%$ minimum load
Power Quality	Individual Harmonics	Harmonic magnitude	$\geq 3\%$
	THDv	Total harmonic voltage distortion	$\geq 5\%$
Control	Regulator	Increased duty	$>$ basecase+1
	Capacitor	Increased duty	$>$ basecase+1

Hawaii Electric had to lower daytime voltage to accept more solar

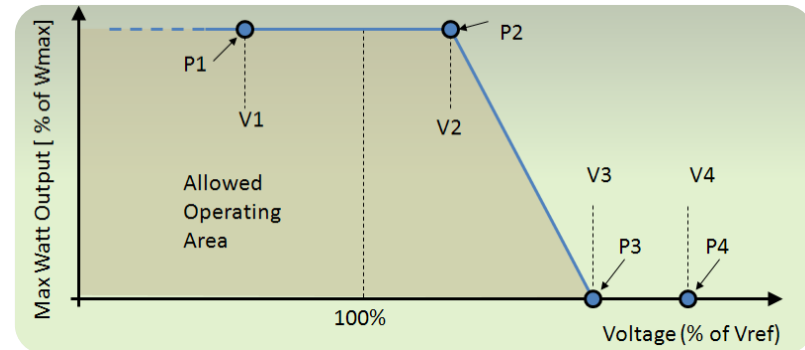


Smart inverters for providing grid support functions will help control voltage

Volt-var Control**



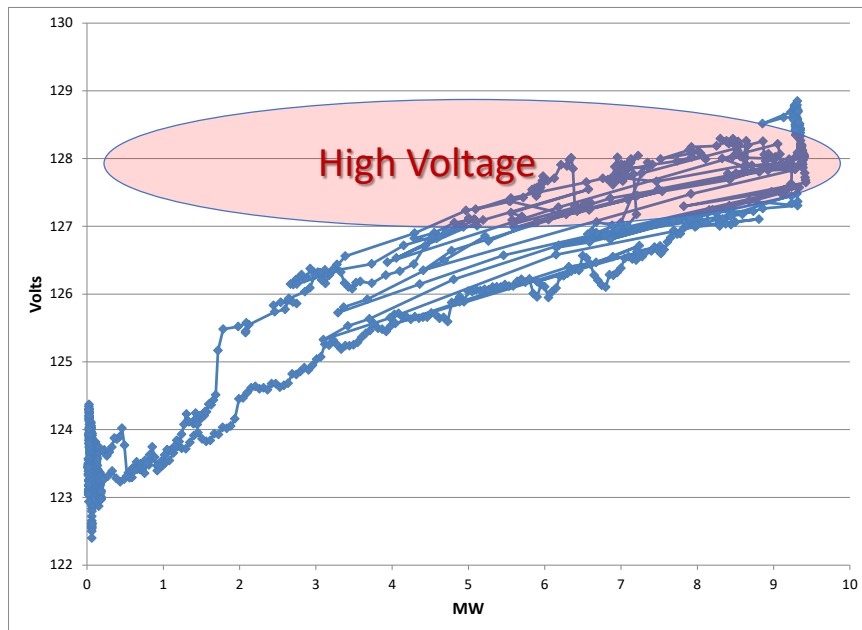
Volt-Watt Control**



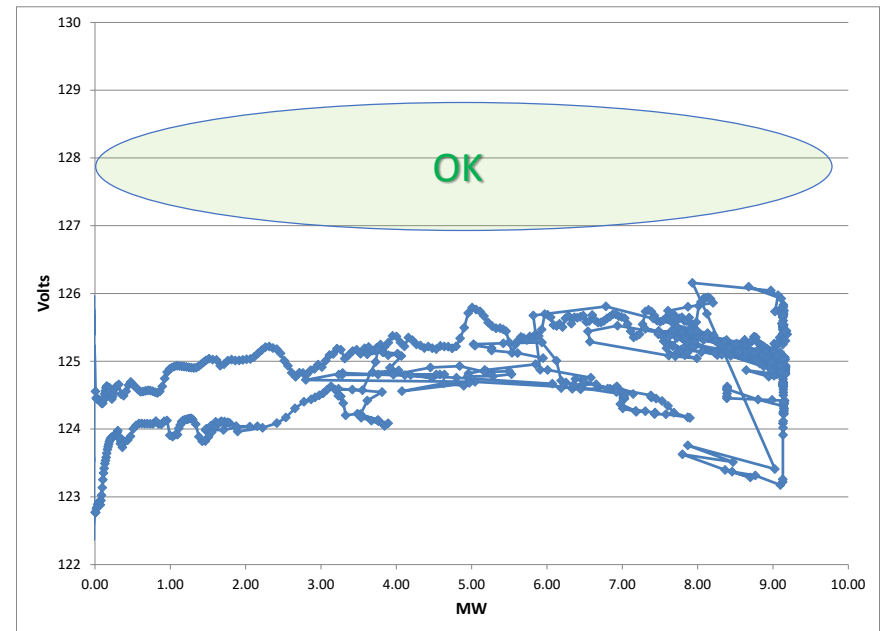
Power factor tuning at some Indiana sites

Had to “tune” power factor at large sites to prevent high voltage problems – also added auto shut off

Before Tuning



After tuning



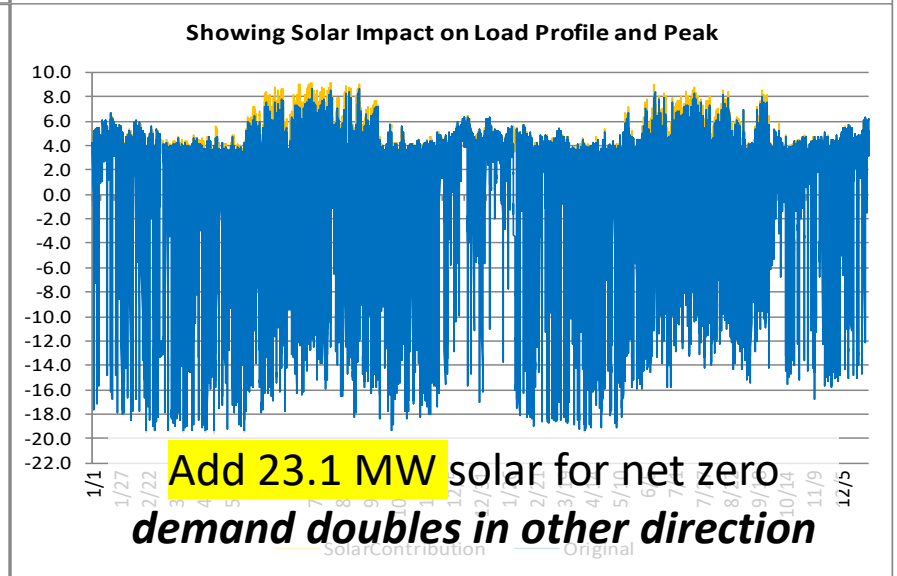
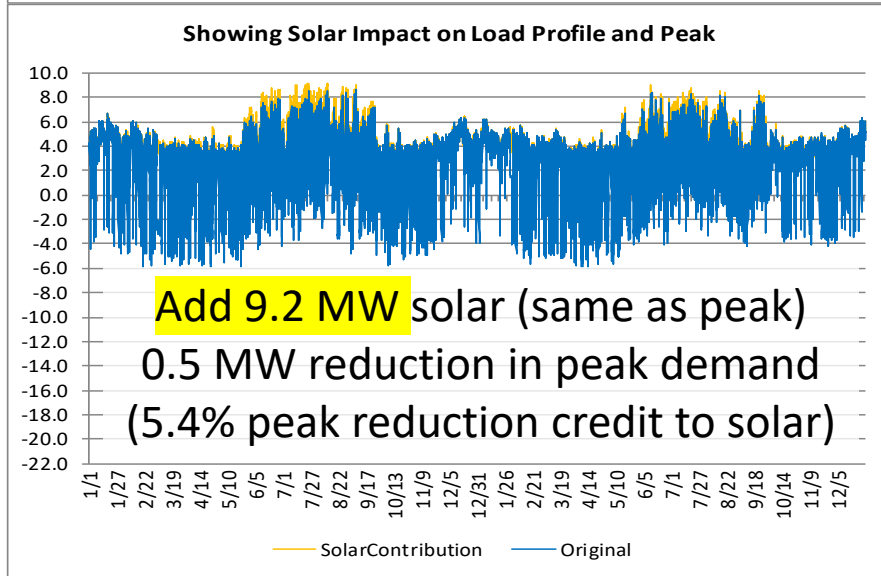
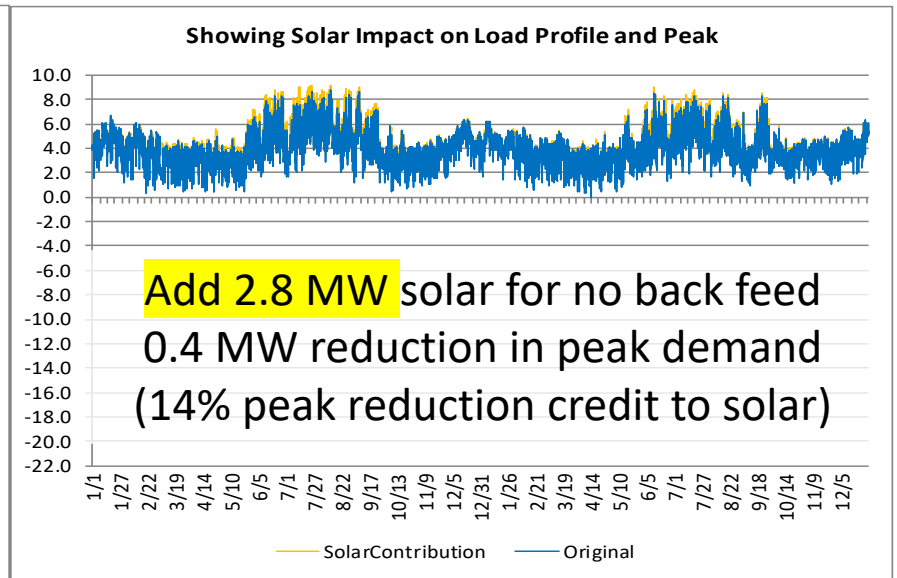
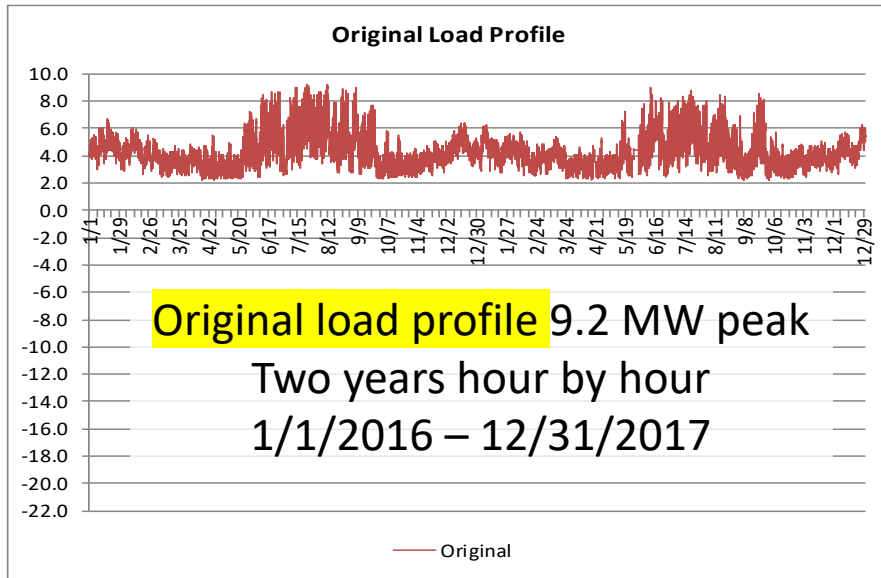
Recent change in C84.1 for renewables

- C84.1 is the longstanding standard for voltage
 - All the way from the generator to the wall outlet
 - Nominal voltage
 - Maximum and minimum voltages
- IEEE 1547 may have introduced some confusion
 - Sets continuous overvoltage trip setting at 110%
 - C84.1 Range A is 105%
 - 1547 requires DR to keep Range A at point of common coupling but it is not clear how to do it.
- Challenged appliance and equipment suppliers to consider allowing higher voltage in C84.1
 - All opposed the change
 - Adding an annex suggesting *5% rise only in dedicated circuits*

Why do what would have happened model

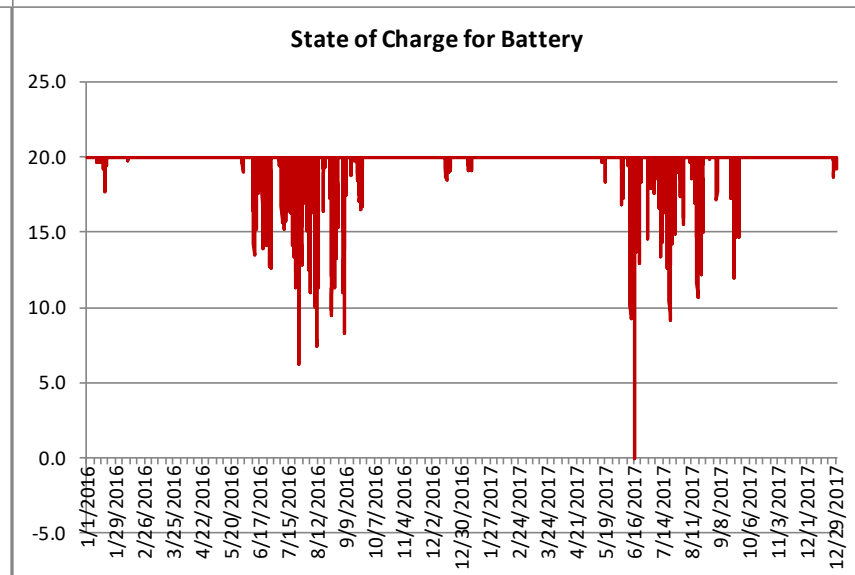
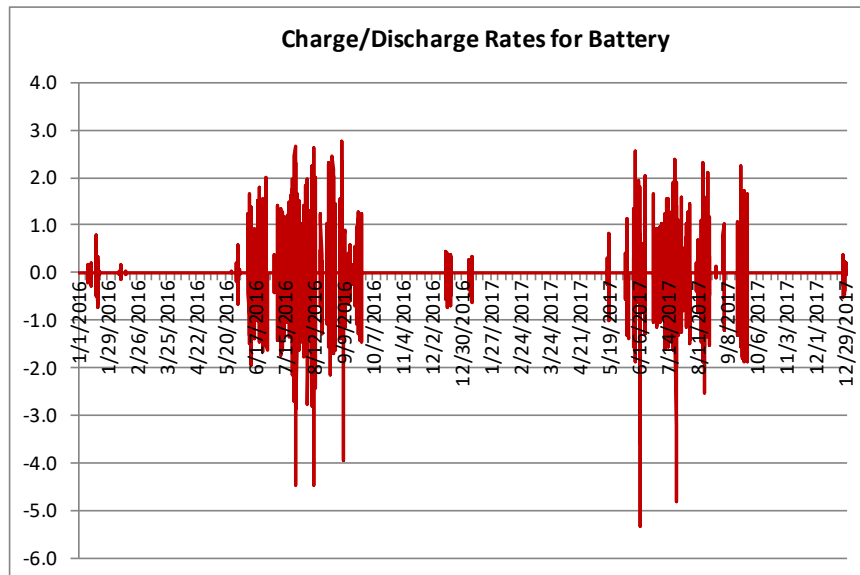
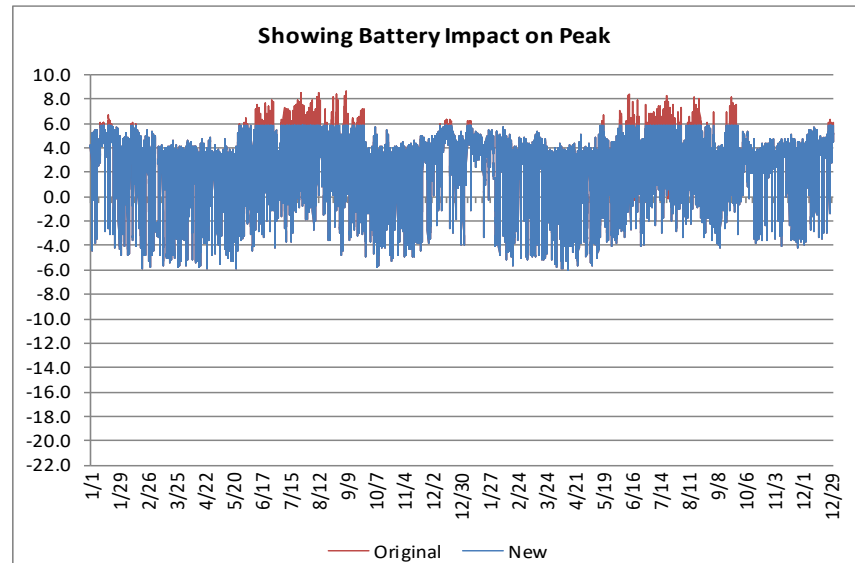
- Many years observing solar output and sending it to State Utilities Forecast Group
- Observed occasional coincident low output of intermittent resources (wind and solar)
- Concern that traditional peak load resource models were no longer adequate
- Needed a simplistic way to understand what could happen
 - Building tools in Excel workbooks so it is easily understood
 - Modeling what would have happened is easier to understand
 - Simulate different resource mixes based on known performance
 - Use what we learn to inform needs for future analysis
- One model for distribution and one for larger systems

Add solar to a summer peaking distribution circuit



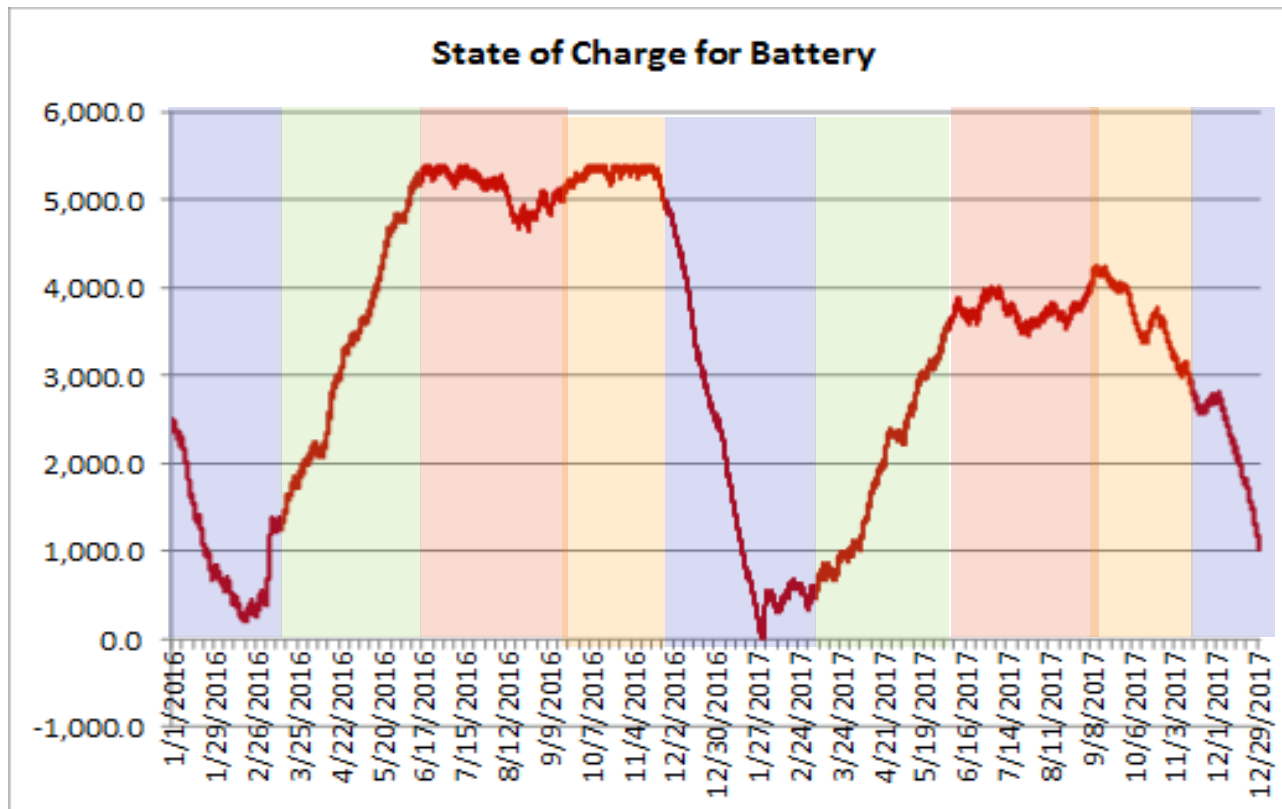
Same circuit 9.2 MW solar & 20 MWh battery

- Try adding 20 MWh battery and 9.2 MW of solar for circuit with 9.2 MW demand
- Peak demand dropped to from 9.2 MW to 5.9 MW
- Use battery only for peak reduction (not daily smoothing)



Net zero or microgrid with only solar and battery

- 9.2 MW summer peaking circuit
- Needs 23 MW of solar and 5,380 MWh of battery (~400,000 Tesla PW II)
- Battery is best described as seasonal rather than daily or hourly



User inputs to Excel workbook bulk model

- 5-year actual coincident history in ***per unit*** of rated capacity and of peak load
 - Load profile (using MISO Midwest in examples)
 - Wind production (using MISO wind performance)
 - Solar (using central Indiana in examples)
- Accepts any resource mix in MW and MWh
 - Dispatchable (typically fossil) assumes 100% credit
 - Wind – inputs rated MW and estimates MISO capacity credit
 - Solar – inputs rated MW and estimates MISO capacity credit
 - Battery MWh - charge/discharge rate assumes 4-hour with no round trip losses
- Always uses renewables and battery before dispatchable
- Review one example in detail – then three more side by side comparisons
- All examples use 1,000 MW peak load, and all graphs use the same scale for good visual comparison

How the model works

Avg Energy MWh	4,637,767	LF	53%	Peak Load Input	Solar	Wind	Battery (4 Hr Dur)	Fossil	Total Annual Fixed Charges at 15% LFCR	Avg Annual Energy Cost	Total Capacity, Open Capital Inv	
Avg Fossil MWh	2,988,726	LF	42%	1,000	400	400	100	815			1,715	Installed M
Avg Renewable MWh	1,649,041	LF	24%	Cost / kW or kWh	\$ 1,000	\$ 1,400	\$ 200	\$ 1,100	\$ 281	\$ 159.40	1,103	Credit MW
Avg Renew Curtail MWh	3,651	PCT Ren	36%	Capital \$M	\$ 400	\$ 560	\$ 20	\$ 897	Average cost per kWh		10%	Reserves
Battery discharge rate	25%	25	MWh	Energy /\$ MWh	\$ -	\$ -	\$ -	\$ 32.00	\$ 0.0951	per kWh	\$ 441	M\$ Annual
				~ MISO Capacity	200	63	25	815	1,103	Total MISO	\$ 1,877	M\$ Total C
Date /Time EST Hour Ending	Load PU of Peak	Wind PU of Rated	Solar PU of Rated	Model Load	Model Solar Available	Model Wind Available	Wind and Solar Excess	Stored Amount	Battery Contribution	Fossil Dispatch	Total Resource	Excess / Shortage
3/22/15 10:00	0.536	0.542	0.086	536	34	217	-284	0	0	284	536	0
3/22/15 11:00	0.535	0.573	0.366	535	146	229	-159	0	0	159	535	0
3/22/15 12:00	0.531	0.568	0.712	531	285	227	-19	0	0	19	531	0
3/22/15 13:00	0.525	0.549	0.906	525	362	219	57	25	-25	0	557	32
3/22/15 14:00	0.517	0.566	0.947	517	379	226	89	50	-25	0	580	64
3/22/15 15:00	0.512	0.554	0.949	512	380	222	90	75	-25	0	576	65
3/22/15 16:00	0.511	0.527	0.978	511	391	211	91	100	-25	0	577	66
3/22/15 17:00	0.517	0.528	0.964	517	386	211	80	100	0	0	597	80
3/22/15 18:00	0.525	0.516	0.819	525	328	207	9	100	0	0	534	9
3/22/15 19:00	0.538	0.520	0.457	538	183	208	-147	75	25	122	538	0
3/22/15 20:00	0.572	0.545	0.277	572	111	218	-243	50	25	218	572	0
3/22/15 21:00	0.572	0.586	0.055	572	22	234	-315	25	25	290	572	0
3/22/15 22:00	0.553	0.609	0.000	553	0	244	-310	0	25	285	553	0
3/22/15 23:00	0.527	0.587	-0.002	527	-1	235	-293	0	0	293	527	0
3/23/15 0:00	0.507	0.556	-0.002	507	-1	222	-285	0	0	285	507	0

Per Unit Values
System Peak
Renewable
Nameplate

Calculated Load
and Renewable
Output

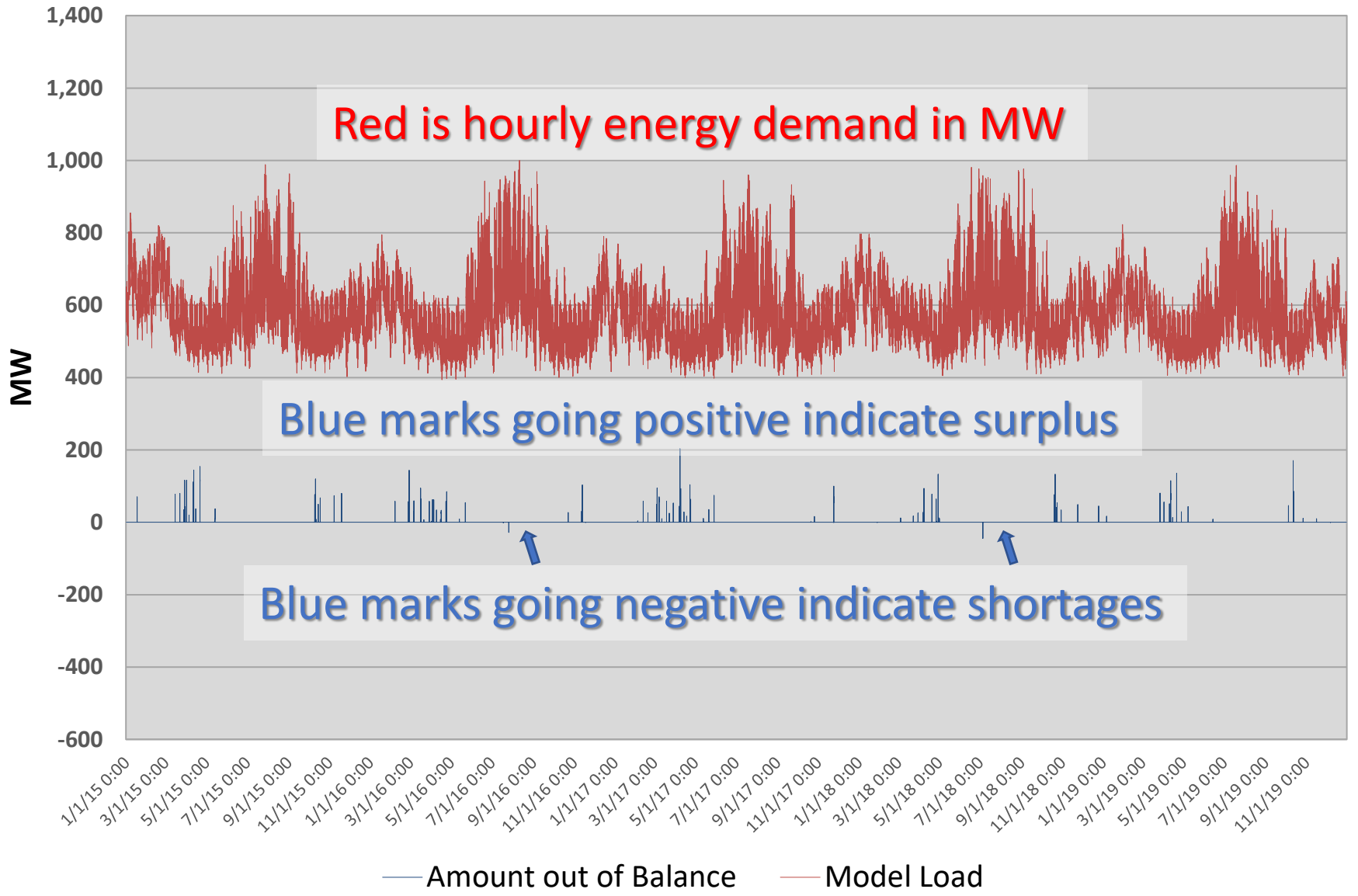
Resource & Battery Dispatch
Uses Fossil as Last Resort

Sample detail outputs follow

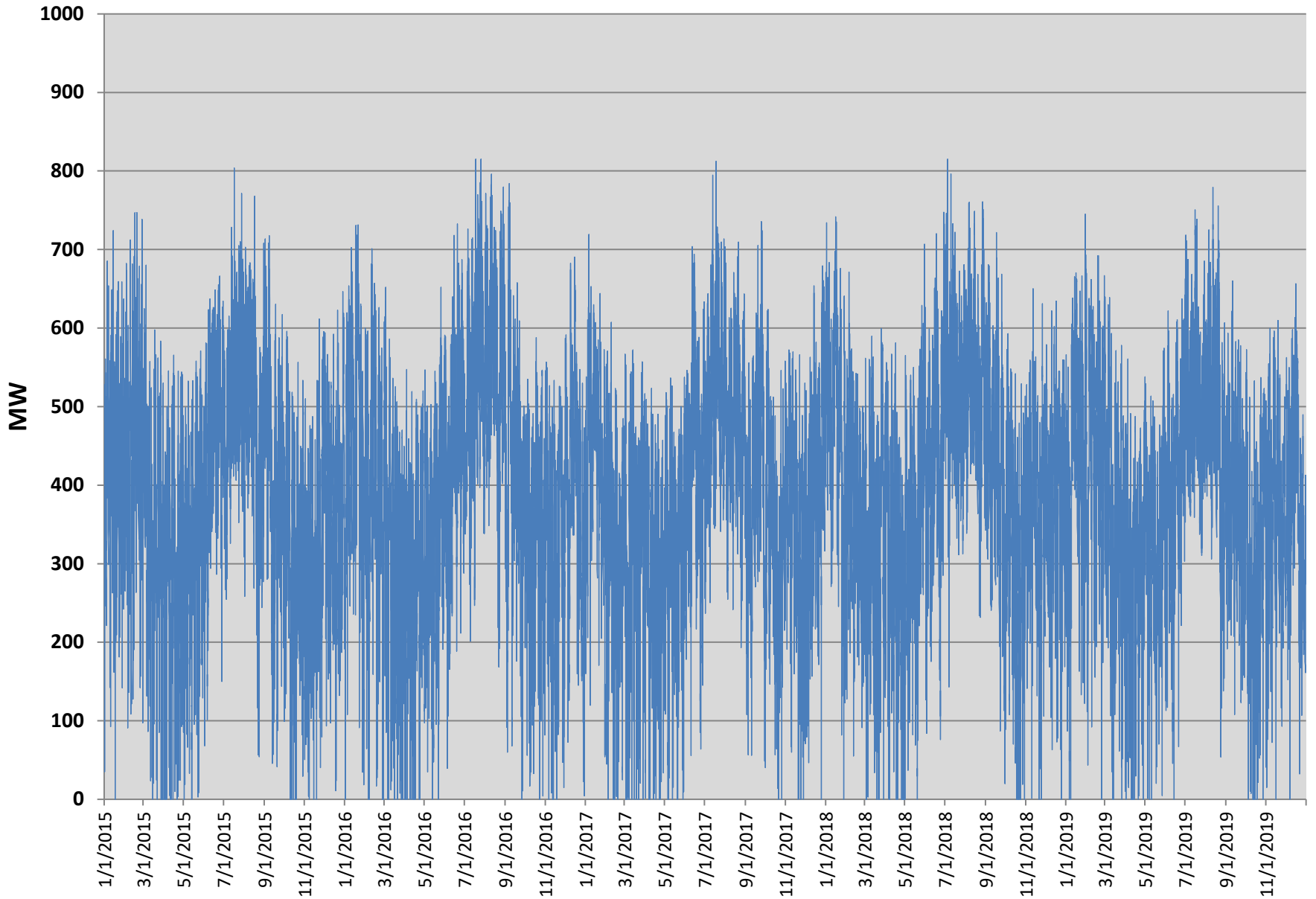
- Use inputs from the previous slide
- Outputs are as large as possible (No slide headings)
- Output slides to follow in order
 - Traditional load and control area error shows hourly load profile and how much one entity will be leaning on neighbors
 - Output from dispatchable resources
 - Hourly percent of customers possibly without power if no external resources are available
 - Average number of days of shortage per year by month and hour of day
 - Coincident output of wind and solar for 5 years
 - Battery state of charge

Traditional Load and Area Control Error by Hour 2015 through 2019

(Blue is leaning on neighbors to avoid renewable curtailment or rotating blackouts)

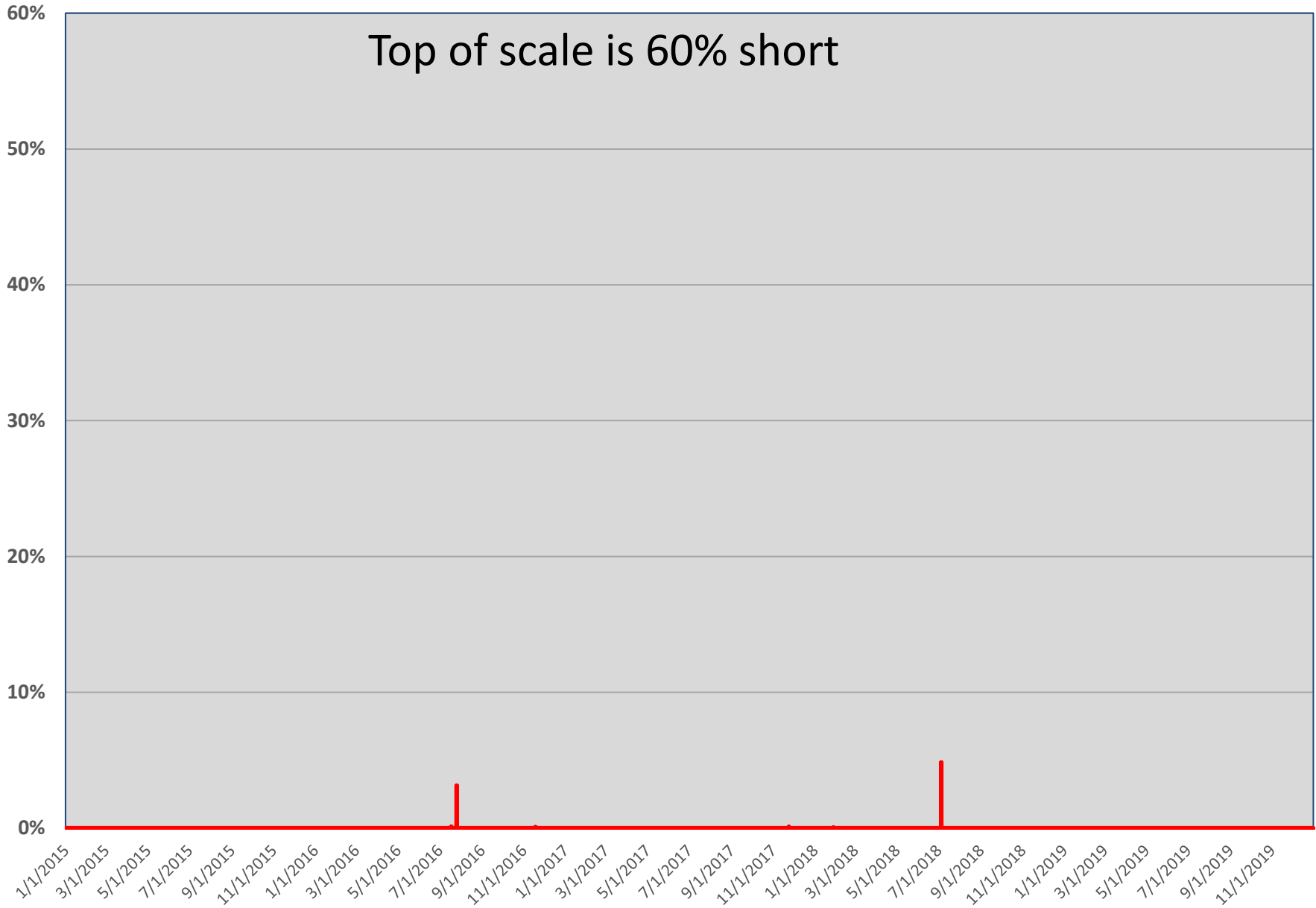


Dispatchable Output (Traditionally Fossil)

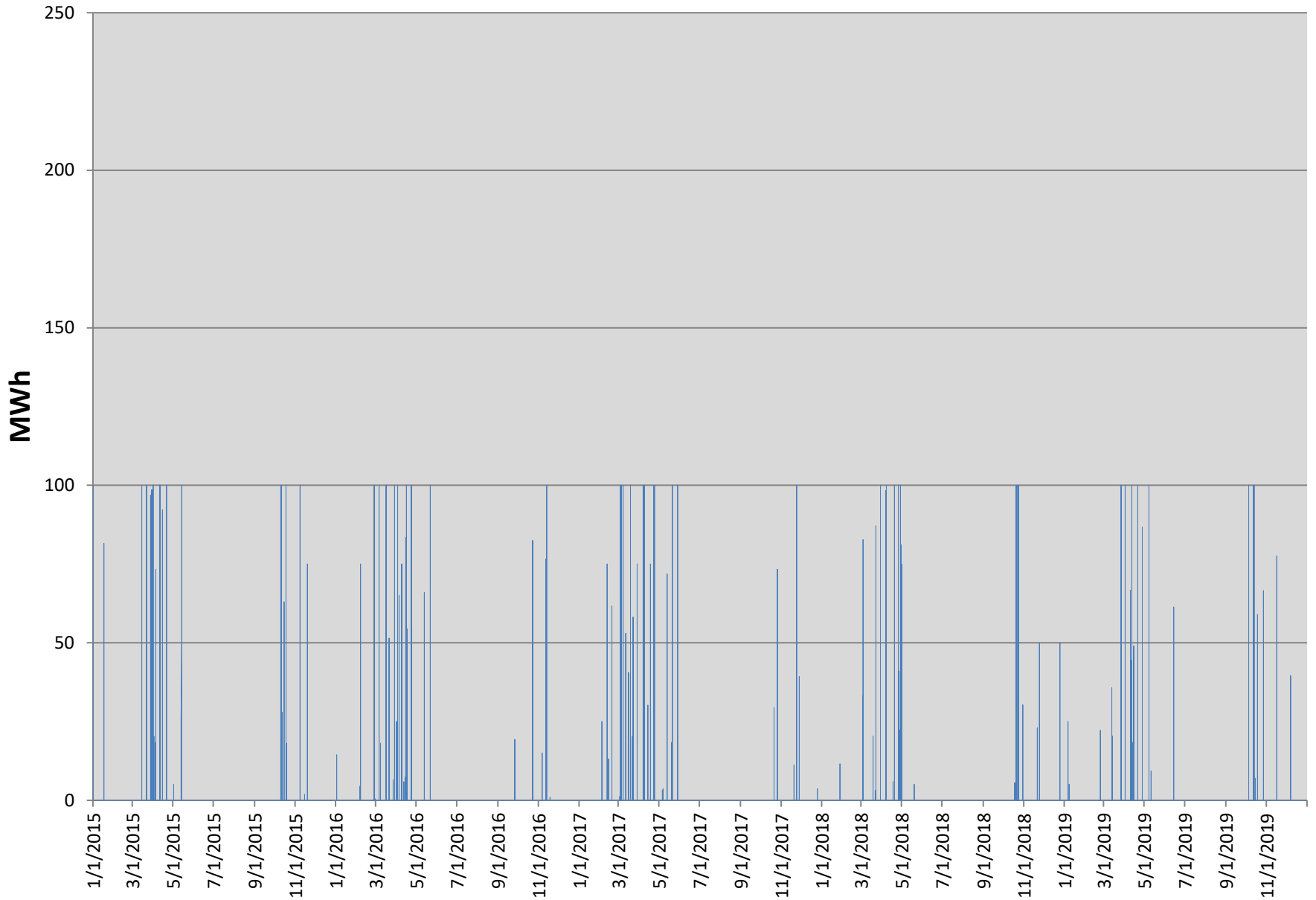


Percent Power Shortage Hour by Hour - 2015 through 2019

Top of scale is 60% short



Battery State of Charge



Run four scenarios to illustrate differences

Scenario 1

This is previous example

Solar	400
Wind	400
Battery	100
Dispatchable	815
Total Nameplate	1,715

Scenario 2

Solar	1,000
Wind	1,000
Battery	200
Dispatchable	500
Total Nameplate	2,700

Scenario 3

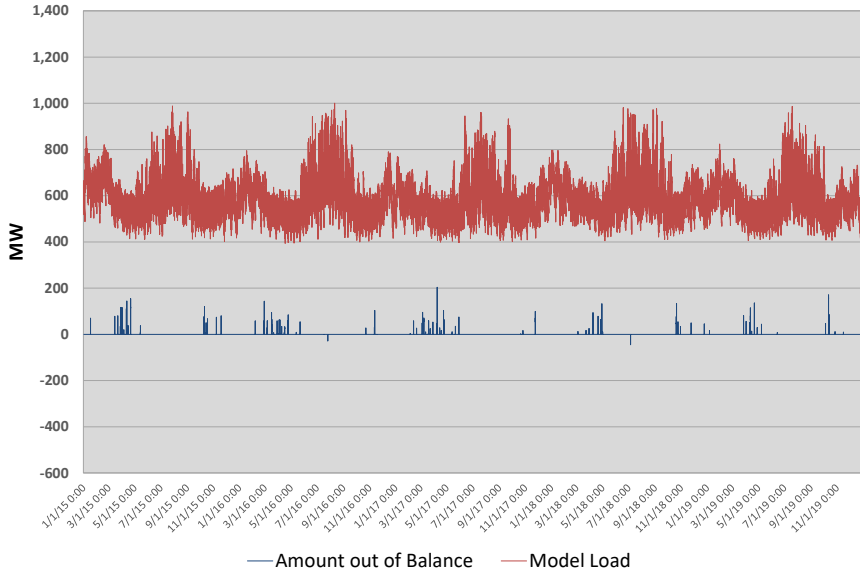
Solar	1,008
Wind	319
Battery	106
Dispatchable	761
Total Nameplate	2,195

Scenario 4

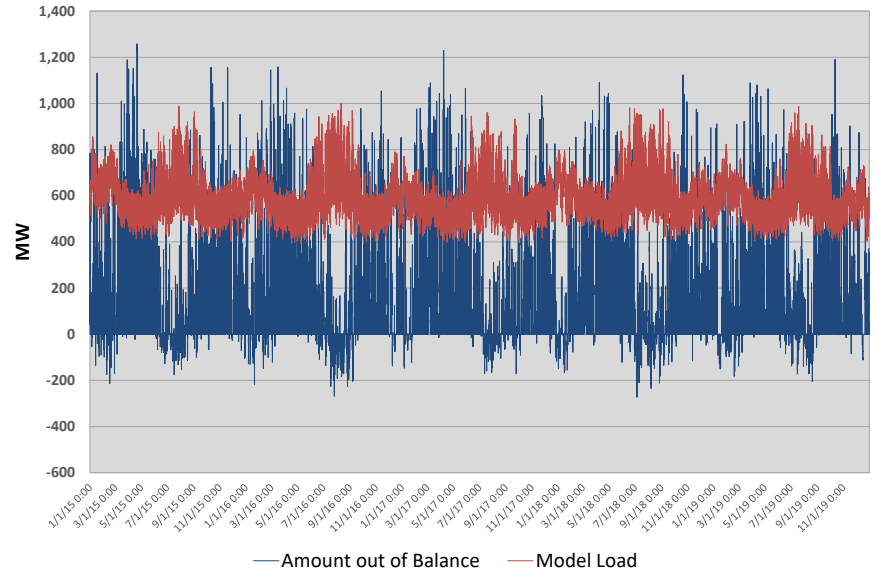
Solar	1,303
Wind	567
Battery	170
Dispatchable	320
Total Nameplate	2,360

All scenarios serve the same load profile with 1,000 MW peak
Results will be in the same quadrants as the inputs on slides

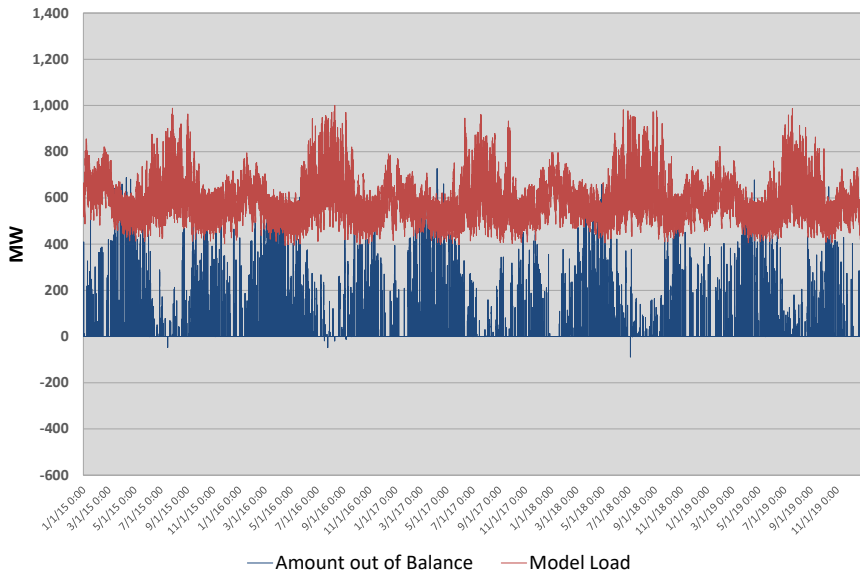
Traditional Load and Area Control Error by Hour 2015 through 2019
(Blue is leaning on neighbors to avoid renewable curtailment or rotating blackouts)



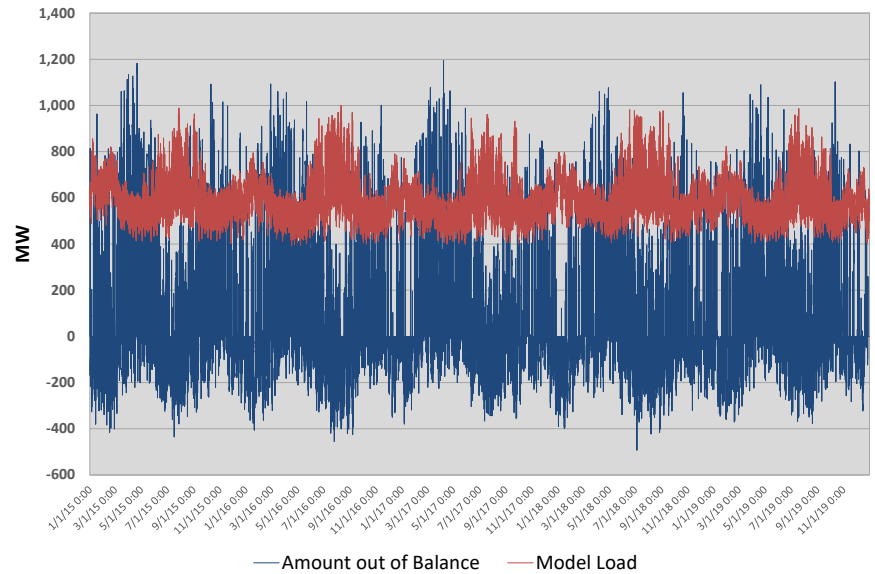
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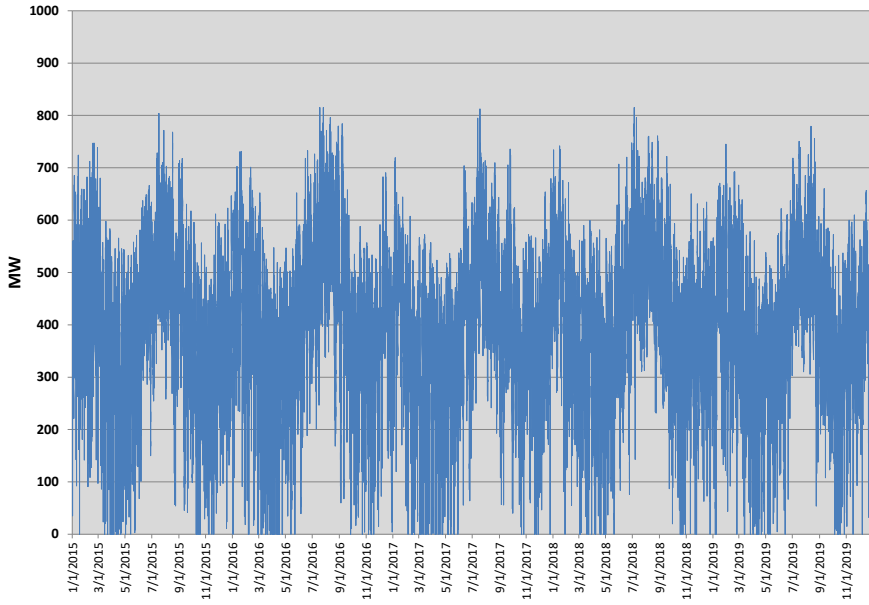
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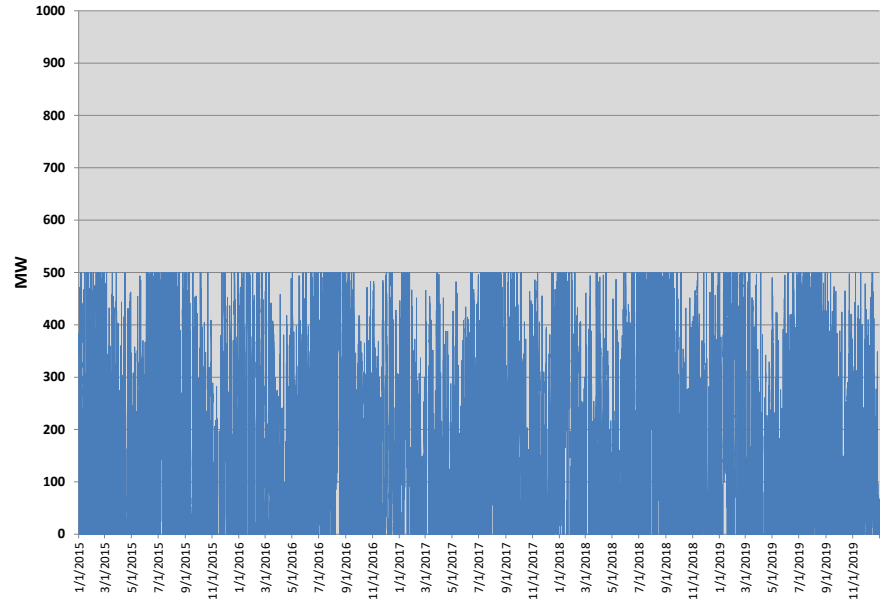
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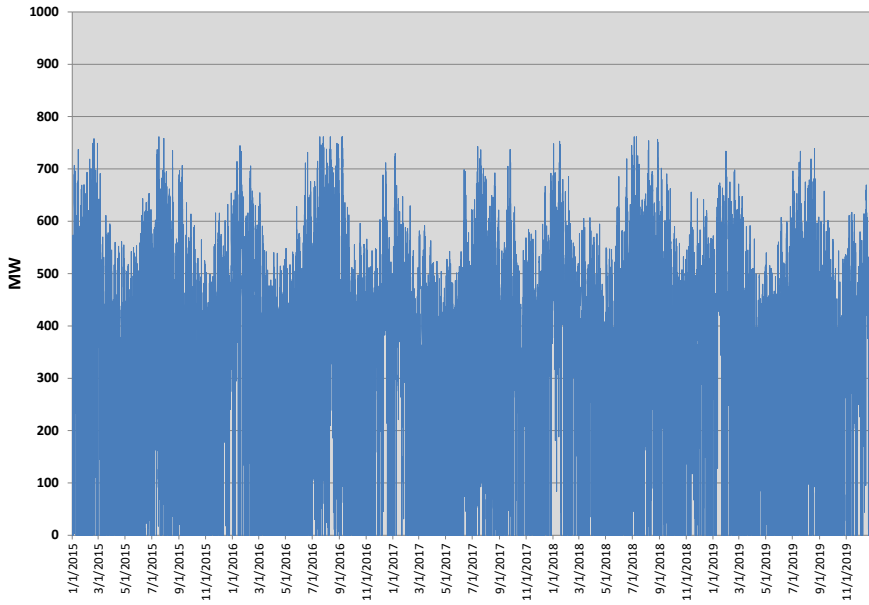
Dispatchable Output (Traditionally Fossil)



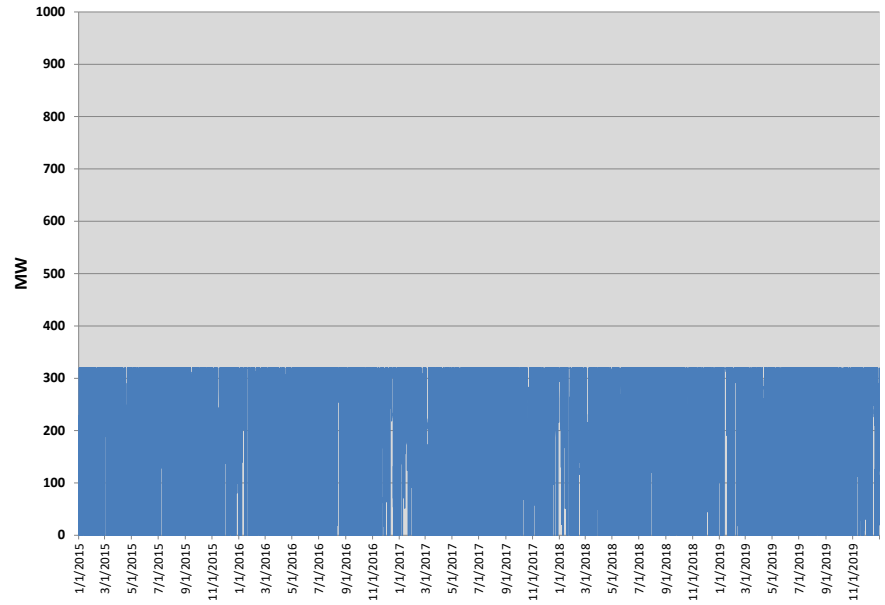
Dispatchable Output (Traditionally Fossil)



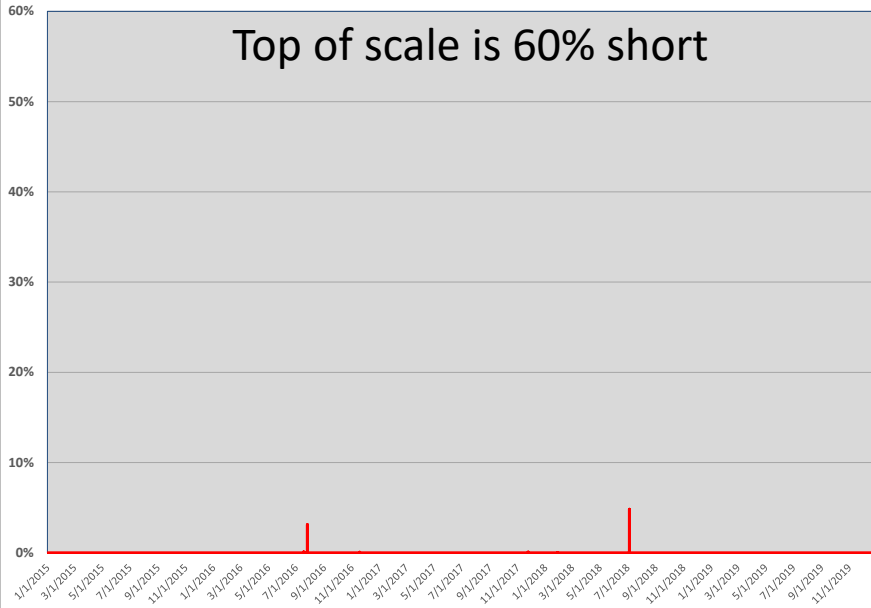
Dispatchable Output (Traditionally Fossil)



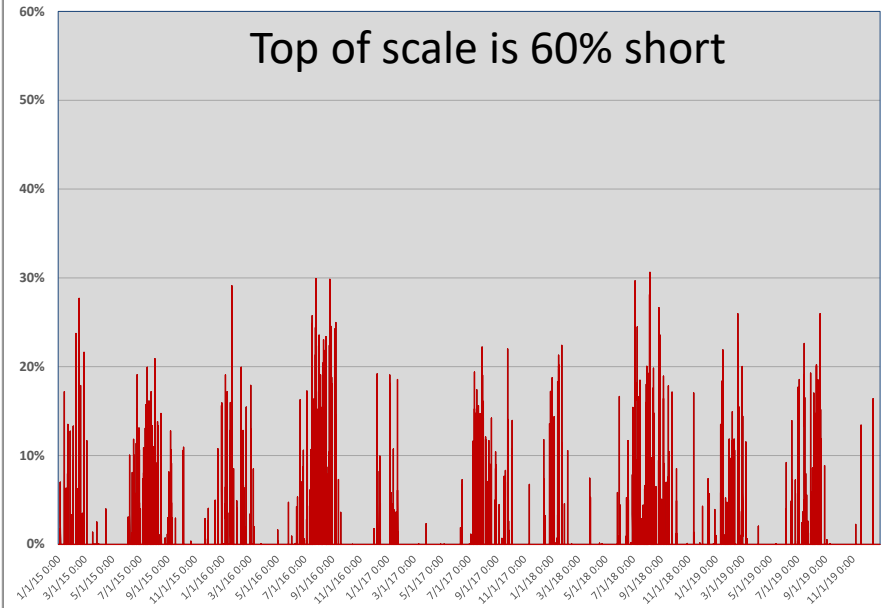
Dispatchable Output (Traditionally Fossil)



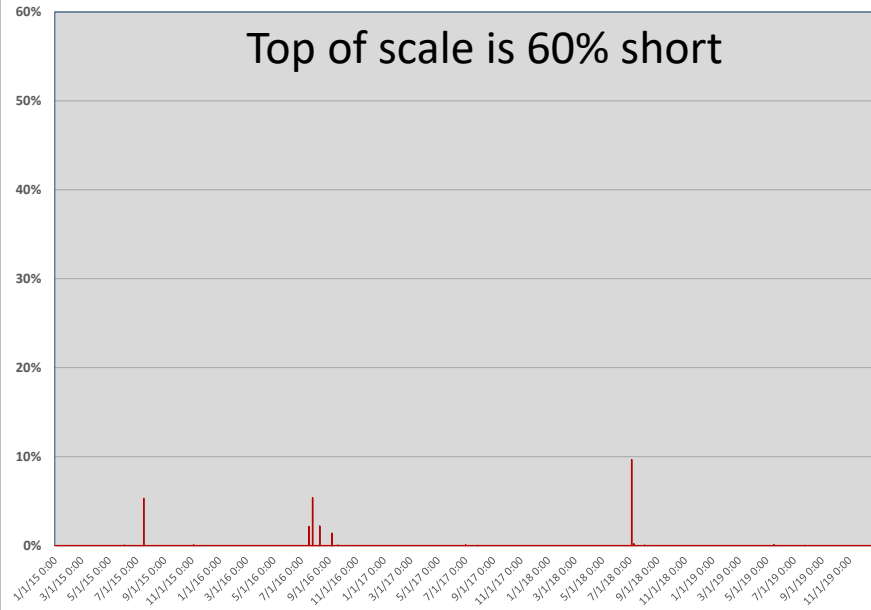
Percent Power Shortage Hour by Hour - 2015 through 2019



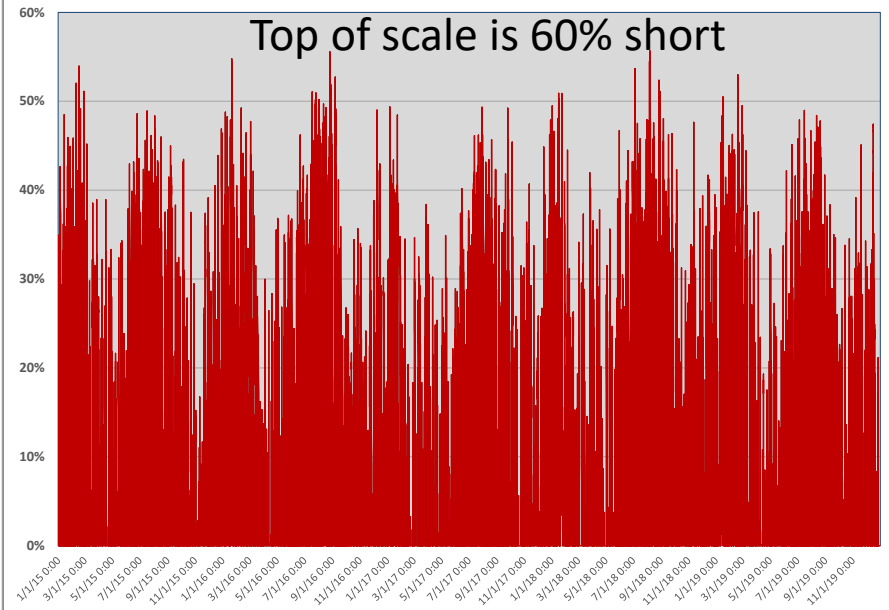
Percent Power Shortage Hour by Hour - 2015 through 2019



Percent Power Shortage Hour by Hour - 2015 through 2019



Percent Power Shortage Hour by Hour - 2015 through 2019



Average number of days short of supply per year

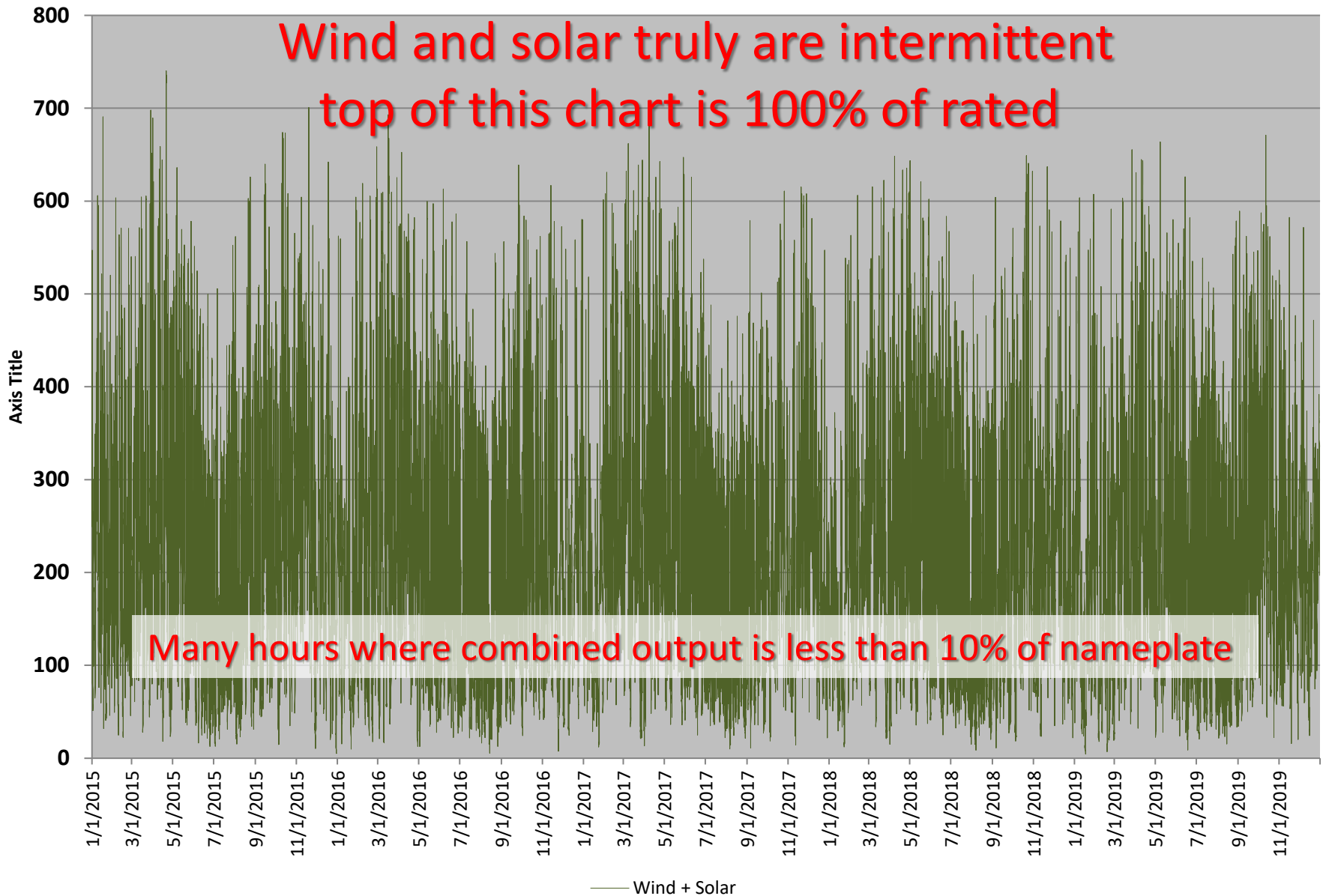
Days Short per Year		Month												Days Short per Year		Month																																				
		1	2	3	4	5	6	7	8	9	10	11	12			1	2	3	4	5	6	7	8	9	10	11	12																									
Hour Ending	1	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	Hour Ending	1	1.2	0.2	0.2	0.0	0.0	0.4	0.6	1.8	0.2	0.0	0.0	0.4	Hour Ending	1	19.4	12.2	8.6	4.8	10.8	19.6	28.2	26.6	13.4	6.6	8.8	10.8
	2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		2	0.8	0.2	0.2	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0		2	17.6	11.6	8.8	4.4	8.4	17.8	26.8	25.4	12.4	5.6	8.4	10.6
	3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		3	0.8	0.4	0.2	0.0	0.0	0.0	0.0	0.4	0.0	0.0	0.0	0.0		3	18.2	11.8	9.4	4.6	8.0	16.4	26.4	24.0	12.0	4.8	8.6	10.6
	4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		4	0.8	0.4	0.2	0.0	0.0	0.0	0.0	0.6	0.0	0.0	0.0	0.0		4	18.0	13.0	10.6	5.8	8.6	16.2	26.6	24.4	12.4	6.4	8.2	10.4
	5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		5	1.0	1.0	0.2	0.0	0.0	0.2	0.2	1.2	0.0	0.0	0.0	0.0		5	18.2	13.2	12.2	8.0	10.0	17.6	27.6	26.0	14.4	9.4	9.6	11.6
	6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		6	2.0	2.0	0.2	0.0	0.0	0.6	0.6	3.2	0.2	0.0	0.0	0.0		6	19.0	14.8	16.2	11.2	14.6	19.8	28.8	27.2	18.2	12.2	13.0	14.2
	7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		7	4.2	3.0	1.6	0.0	0.0	1.6	3.2	5.6	0.8	0.6	0.0	1.2		7	21.4	17.8	19.0	13.2	18.2	24.2	29.8	28.2	21.0	15.0	14.2	17.8
	8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		8	5.8	3.8	2.0	0.0	0.2	4.2	8.4	10.6	1.2	1.0	0.2	2.2		8	24.0	19.4	19.0	14.6	20.4	26.2	30.6	29.2	23.4	15.4	15.2	20.4
	9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		9	6.4	3.8	2.2	0.2	0.2	3.8	11.6	15.8	3.6	0.8	0.4	2.6		9	25.2	19.8	19.6	14.8	16.2	23.8	30.0	29.6	25.8	18.4	15.4	20.8
	10	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		10	5.0	2.4	1.4	0.2	0.0	1.4	4.6	9.2	2.6	0.8	0.2	2.2		10	23.6	13.8	14.0	5.8	5.8	8.8	19.2	24.6	20.8	15.0	9.0	18.6
	11	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		11	3.2	1.0	0.6	0.0	0.0	0.6	1.6	3.8	1.2	0.4	0.2	1.4		11	14.6	9.2	7.6	2.0	3.2	3.6	6.4	9.4	5.8	6.8	5.8	11.8
	12	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		12	2.6	0.8	0.2	0.0	0.0	0.0	0.8	2.6	0.4	0.0	0.0	0.8		12	11.6	6.0	3.8	1.6	1.0	2.8	3.8	5.6	2.8	3.2	3.6	8.6
	13	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		13	2.4	0.4	0.0	0.0	0.0	0.0	0.8	1.4	0.4	0.2	0.0	0.6		13	9.2	4.4	2.8	0.2	0.4	1.2	2.2	5.0	1.8	2.2	2.8	6.4
	14	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		14	2.0	0.6	0.0	0.0	0.2	0.0	1.4	1.6	0.2	0.0	0.2	0.6		14	8.2	3.0	1.4	0.2	0.6	1.2	2.4	3.2	1.4	1.0	2.0	5.6
	15	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		15	1.6	0.6	0.0	0.0	0.2	0.0	1.0	1.4	0.0	0.0	0.2	0.4		15	8.6	2.8	1.2	0.0	0.2	1.2	2.6	2.2	0.8	1.2	2.2	5.8
	16	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		16	1.8	0.4	0.0	0.0	0.0	0.0	0.8	1.2	0.0	0.2	0.2	0.4		16	8.6	3.2	1.4	0.2	0.0	0.8	2.0	2.2	1.2	1.6	2.4	6.8
	17	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		17	2.0	0.4	0.0	0.0	0.0	0.0	1.0	1.4	0.0	0.0	0.2	0.4		17	11.4	3.6	2.0	0.2	0.4	1.6	3.0	2.6	1.8	2.0	4.0	8.6
	18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		18	3.4	1.2	0.0	0.0	0.0	0.0	1.0	1.8	0.2	0.0	0.8	1.8		18	17.2	7.0	2.4	0.2	0.2	1.6	4.6	2.8	2.4	2.6	8.6	15.2
	19	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		19	5.8	1.8	0.6	0.0	0.0	0.4	2.4	1.6	0.4	0.2	0.8	2.2		19	24.4	14.0	4.8	0.6	1.0	2.0	5.8	6.0	3.4	4.8	15.4	21.0
	20	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		20	5.4	4.0	0.6	0.0	0.2	0.4	3.4	4.4	1.8	0.4	0.8	1.8		20	26.0	19.8	9.8	1.8	2.0	4.4	9.8	13.0	10.2	11.6	15.4	19.8
	21	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		21	5.4	3.0	0.8	0.2	0.2	1.0	8.2	10.4	4.0	0.8	1.0	1.0		21	24.2	19.0	12.2	6.0	9.4	15.6	26.2	28.4	20.0	13.2	14.0	18.2
	22	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		22	4.6	2.4	0.6	0.2	0.6	4.4	11.6	11.6	2.6	0.6	0.4	0.6		22	23.8	17.4	12.6	9.8	16.6	24.4	30.2	29.2	19.2	10.2	13.4	17.8
	23	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		23	3.0	2.4	0.2	0.0	0.2	3.4	8.6	7.0	1.0	0.0	0.0	0.6		23	22.4	16.2	10.6	6.6	14.8	23.4	30.0	28.0	16.6	8.4	11.8	15.0
	24	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		24	1.8	1.0	0.2	0.0	0.0	1.6	2.8	3.4	0.4	0.0	0.0	0.6		24	19.8	13.4	9.2	6.0	12.2	21.0	29.0	27.0	16.4	7.0	9.4	12.2

Model results summary for four scenarios

	1	2	3	4
Solar	400	1,000	1,008	1,303
Wind	400	1,000	319	567
Battery	100	200	106	170
Dispatchable	815	500	761	320
Total Nameplate	1,715	2,700	2,195	2,360
Approx Renewable %	36%	74%	44%	58%
Max Percent Out	5%	31%	10%	56%
Max MW shortfall	44	272	89	492
Hours Short Per Year	2	391	4	3,423
Dispatch Stop/Start	28	320	239	312
Curtail MWh	3,651	791,590	241,462	669,037

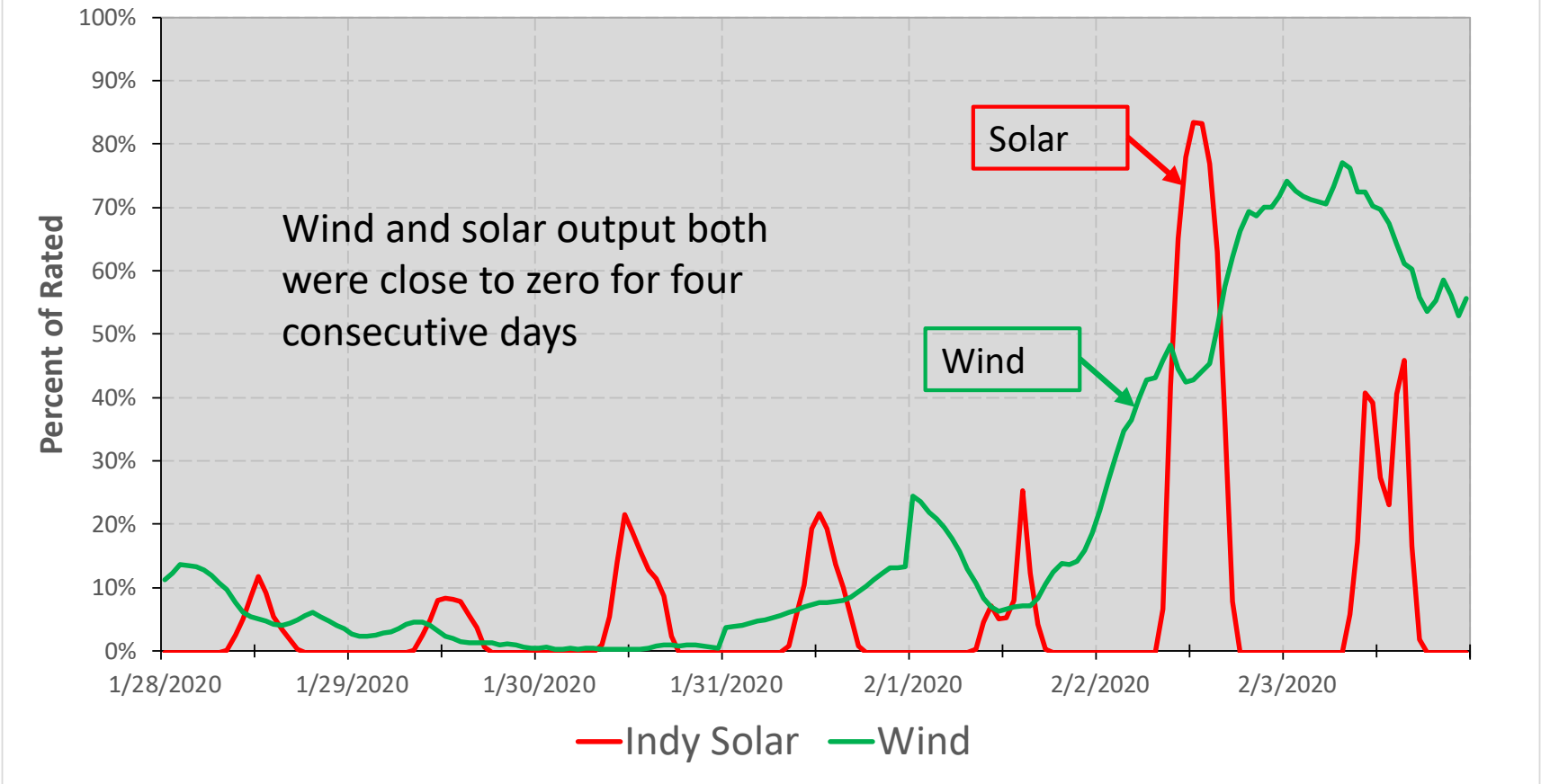
Why do the high dispatchable work better?

Wind + Solar (Scenario 1)

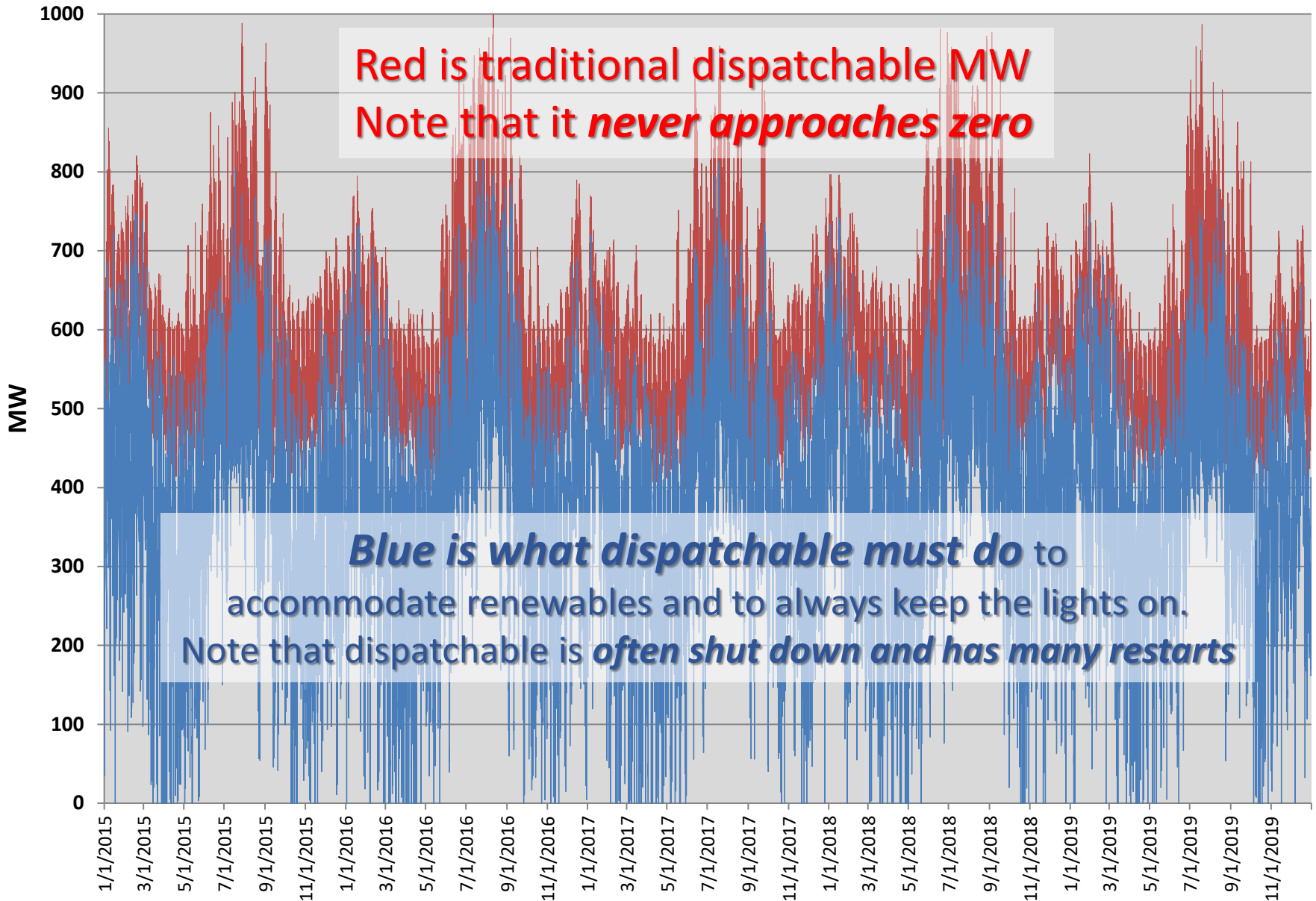


January 2020 central Indiana solar with MISO wind

Central Indiana Solar Production and MISO Wind
Shown in Percent of Rated Capacity
January 28 - February 3 2020



Dispatchable Output (Traditionally Fossil)



Questions?