Current Geotechnical Research Activities to Support Project Delivery & Asset Management

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2025 Midwest Geotechnical Conference

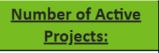
September 23-25, 2025 Sheraton City Centre Hotel, Indianapolis, Indiana





Current Geotech Research



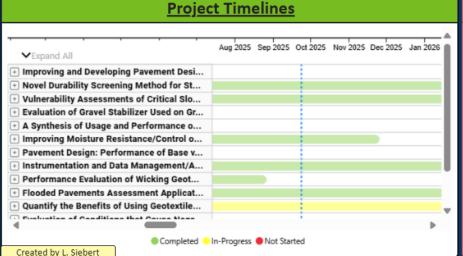


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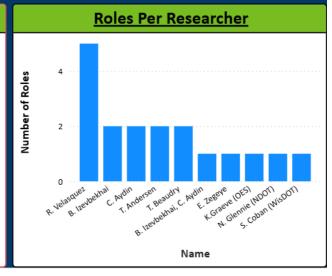
Source MnDOT MnDOT/LRRB NRRA TPF (Iowa DOT)





Current Action Items

- Action item 1:Action item 2:
- Action item 3:

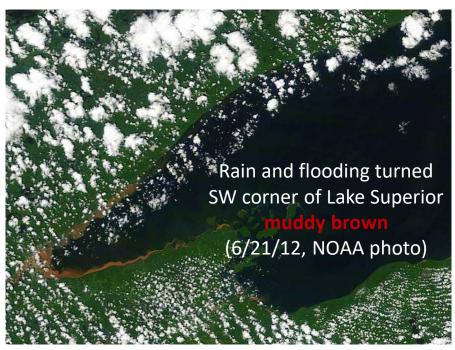


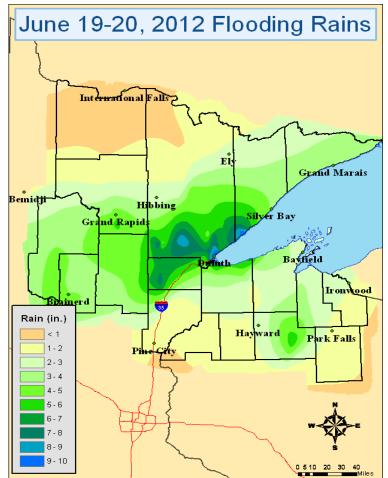
Selected Geotech Research Projects

- 1. Vulnerability Assessment of Slopes
 - Geomorphology-based (WSB)
 - Geotech-based (MSU)
- InSAR for Geotech Asset Management (AUB and TAMU)
- Quantifying Benefits of Geosynthetics for Pavement Foundations (UIUC and ISU)
- 4. RCA (MTU, MSU, Internally)
- 5. Optimization of CSE (Internally)
- 6. Pavement Foundation Uniformity (Internally, Ingios, UTEP)
- 7. Temperature as Surrogate of Pavement Performance (Internally)

Why Slope Vulnerability Assessment?

 Rainy season in June 2012 in Minnesota caused slope failures and major damage in MN Trunk Highway (~\$50 million dollars in damage)





Why Slope Vulnerability Assessment?

- 26 Road Closures on Trunk Highway System
- Major team effort to bring system back:
 - MnDOT, DNR, DPS, Local Law Enforcement, FHWA, Consultants, Contractors.
- MnDOT Main Damage Areas:
 - TH-210 in Jay Cooke
 - TH-210 in Thomson
 - TH-23 in Fond du Lac
 - TH-2 from Proctor to I-35



Goals of Slope Vulnerability Model (Geomorphology-Based)

- Assist engineers to proactively identify and mitigate slope risk along interstate highways
 - Help during <u>project scoping</u> to <u>long range planning</u>
 - Enhance risk-based <u>asset</u>
 <u>management</u> decision making

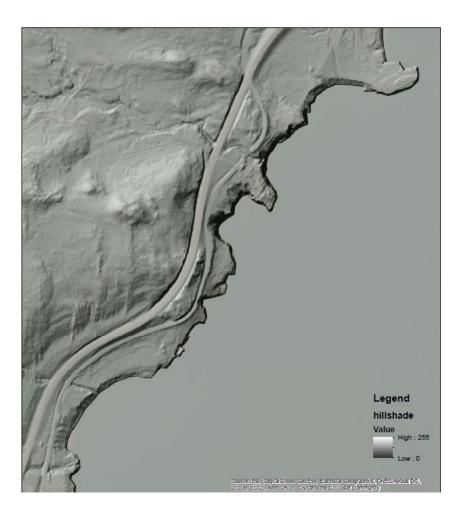




Model assist in proactive identification of slope failures like deep-seated slide in TH-67



Slope Vulnerability Model



Geographic Information Systems (GIS) model that uses:

- Geomorphology of site among other key parameters to provide a <u>vulnerability</u> rating score
- Geographic Weighted
 Regression (GWR) to account
 for local variation of key
 parameters and minimized
 bias and subjectivity

Slope Vulnerability Model

Vulnerability Rating Score is computed with:

$$p = \frac{e^z}{1 + e^z}$$

$$z = \beta_o + \beta_1 X_1 + \dots + \beta_n X_n$$

p = probability of slope failure (0

 X_n =input parameters (independent variables)

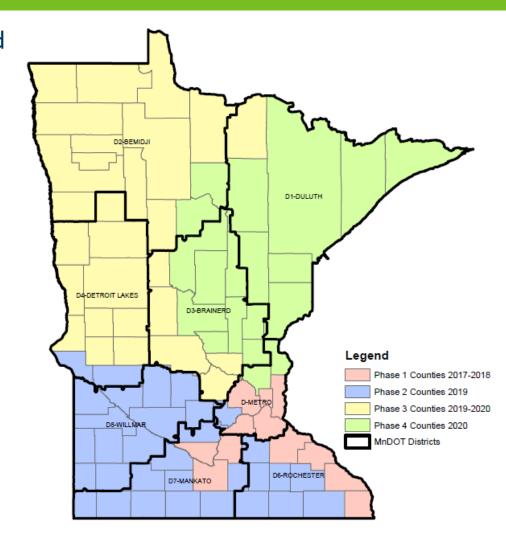
 β_n =regression coefficients from GWR

Model Development

- Selection of preliminary input parameters
 (vulnerability factors) and interaction terms based on
 geomorphology and geology of region
- 2. Checking vulnerability rating using preliminary input parameters and historical slope failures (sensitivity analysis)
- 3. Selecting final input parameters (statistically significant)
- 4. Field verification of model
- Further adjustment (if required)

Model Development

- Phase 1 includes steep terrain and bedrock exposures
- Phase 2 contains steep slopes along river tributaries formed by catastrophic drainage of Glacial Lake Minnesota
- Phase 3 low relief and gradual slopes formed in bed of Glacial Lake Agassiz and glacially eroded and deposited landforms
- Phase 4 small mountain ranges with steep slopes and exposed bedrock and glacial till deposits that form gently rolling terrain



Model Development- Final Input Parameters

Phase 1

- Slope angle
- Terrain curvature
- Distance to streams
- Distance to bedrock outcrops

Phase 2

- Slope angle
- Terrain curvature
- Incision potential
- Local relief

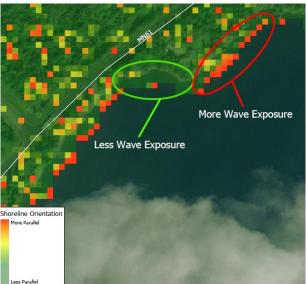
Phase 3

- Slope angle
- Terrain curvature
- Water table depth

Phase 4

- Slope angle
- Slope orientation
- Local relief
- Bedrock proximity
- Elevation



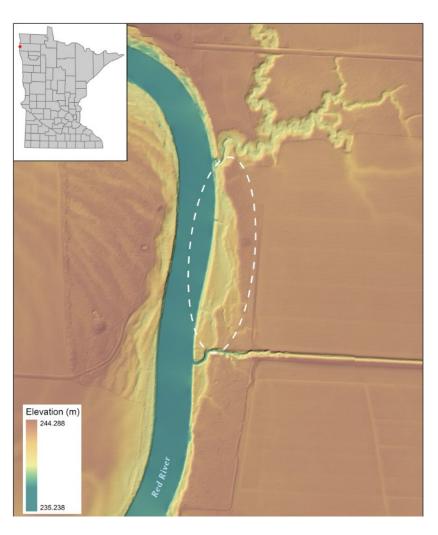




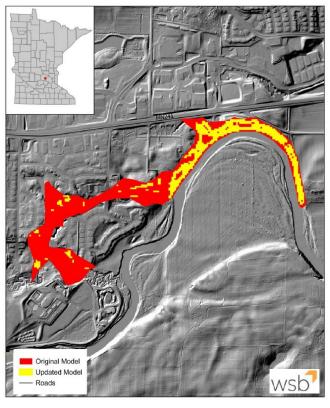
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mndot.gov

Deep-Seated Slide



Field Verification



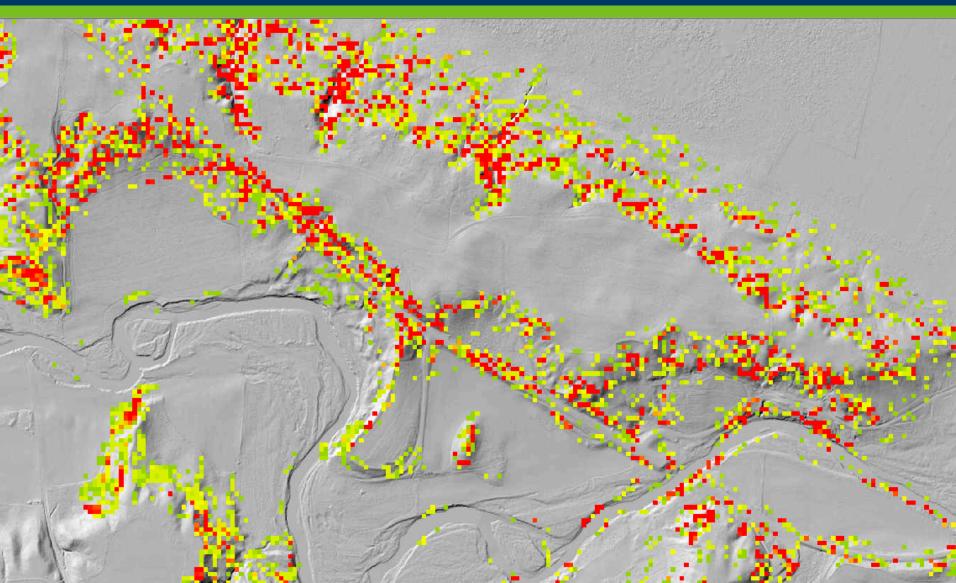






- Validation of final input parameters and vulnerability rating score
- Selection of sites with different geomorphology, geology, and hydrology

Example

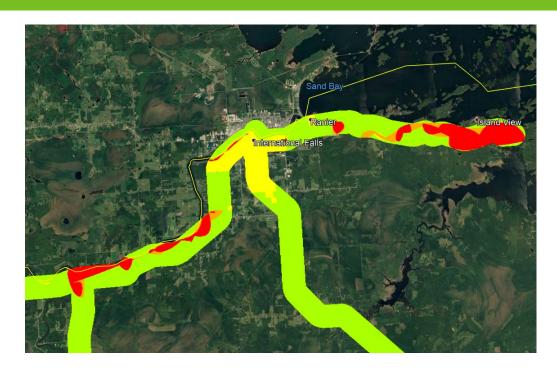


Preliminary Risk Ranking

				Consequence		
				Intersects Trunk Highways	Within 500 feet of Trunk Highways	More than 500 feet of Trunk Highways
				Within Metro or Incorporated Town	Rural	
	Slope Stability	Rational		Critical (5)	Serious (3)	Marginal (2)
LIKELIHOOD	Low	Slope is likely already experiencing mass failure or has the highest risk of failure.	Likely (4)	20 Site Visit / Action Recommended	12 Further Evaluation	8 Monitoring
	Medium	Surface erosion and other pre-cursors for catastrophic failure.	Possible (3)	15 Further Evaluation	9 Monitoring	6 No Action Recommended
	High	Slope has been repaired, recovered, or shows no signs of imminent future.	Unlikely (2)	10 Monitoring	6 No Action Recommended	4 No Action Recommended

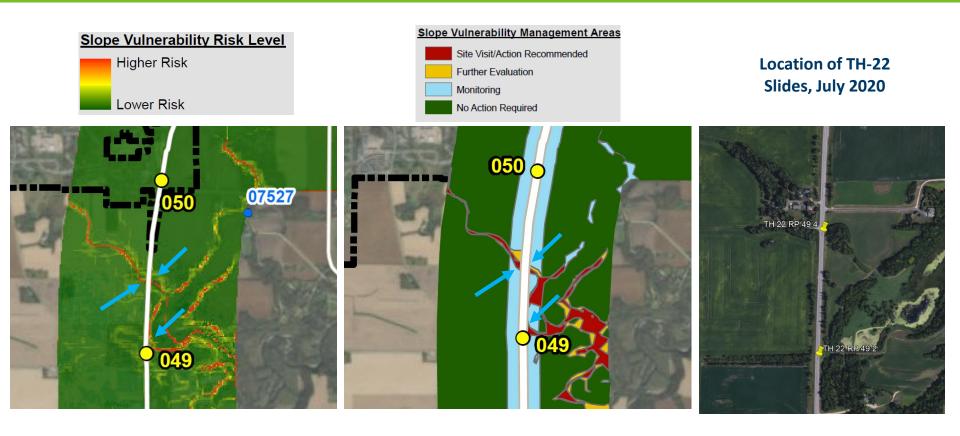
<u>Risk</u> = Likelihood (model output) × Consequence (effect on infrastructure)

Preliminary Risk Ranking



- Risk matrix used to create Preliminary Management Areas
- Preliminary Management Areas => <u>delineated areas in GIS</u>
 with similar risk ranking

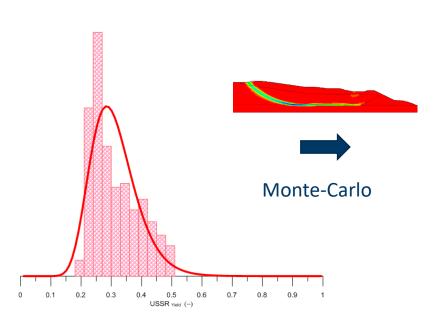
Verification of Model

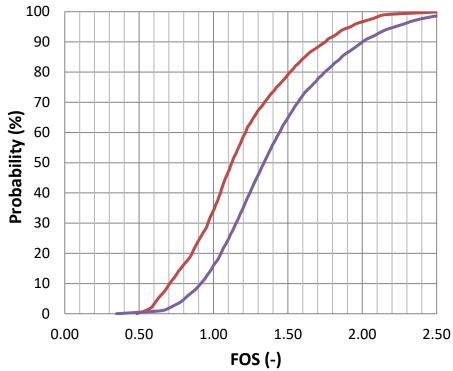


- 1. Address recommendations and gaps from previous studies:
 - MnDOT Slope Vulnerability Phase I-IV
- 2. Help with implementation of advanced geotechnical tools such as 2D and 3D modeling software for slope stability (e.g., PLAXIS 3D)
- 3. Assess value of advanced remote sensing technologies such as UAVs for geotechnical applications
- 4. Improve quantification of risk via powerful numerical methods (commonly available)
- 5. Help with Geotechnical Asset Management (GAM) efforts
- 6. Internal Staff Development

Geotechnical Approach for Slope Assessment

<u>Risk Assessment</u> can be added via powerful numerical methods commonly available:

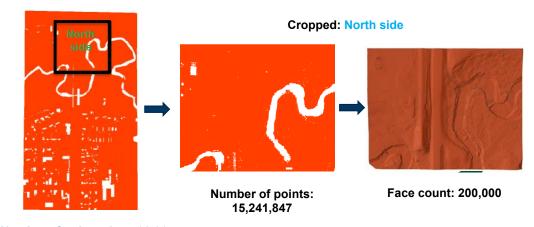




Property or In Situ test results	Coefficient of Variation (CoV) (%)	Source				
Unit weight (γ)	3-7%	Harr (1984), Kulhawy (1992)				
Buoyant unit weight (γ _b)	0-10%	Lacasse and Nadim (1997), Duncan (2000)				
Effective stress friction angle (φ')	2–13%	Harr (1984), Kulhawy (1992)				
Undrained shear strength (Su)	13–40%	Harr (1984), Kulhawy (1992), Lacasse and Nadim (1997), Duncan (2000)				
Undrained strength ratio (S_u/σ^2_v)	5–15%	Lacasse and Nadim (1997), Duncan (2000)				
Compression index (C _c)	10–37%	Harr (1984), Kulhawy (1992), Duncan (2000)				
Preconsolidation pressure (Pp)	10–35%	Harr (1984), Lacasse and Nadim (1997), Duncan (2000)				
Coefficient of permeability of saturated clay (k)	68–90%	Harr (1984), Duncan (2000)				
Coefficient of permeability of partly saturated clay (k)	130-240%	Harr (1984), Benson et al. (1999)				
Coefficient of consolidation (c _v)	33-68%	Duncan (2000)				
Standard penetration test blow count (N)	15–45%	Harr (1984), Kulhawy (1992)				
Electric cone tip resistance (q _c)	5–15%	Kulhawy (1992)				
Mechanical cone tip resistance (qc)	15–37%	Harr (1984), Kulhawy (1992)				
Dilatometer test tip resistance (q _{DMT})	5–15%	Kulhawy (1992)				
Vane shear test undrained strength (S _u)	10–20%	Kulhawy (1992)				
Shear modulus	30 to 90%	Phoon et al. (1995)				
Soil modulus	30 to 90%	Phoon et al. (1995)				
HIHIQUL.guv						

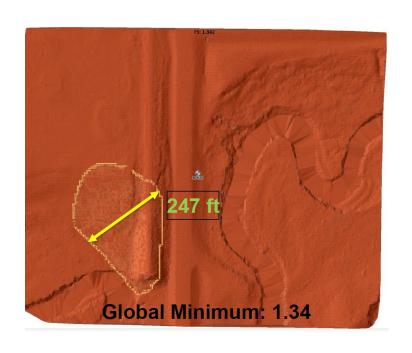
Climax, MN

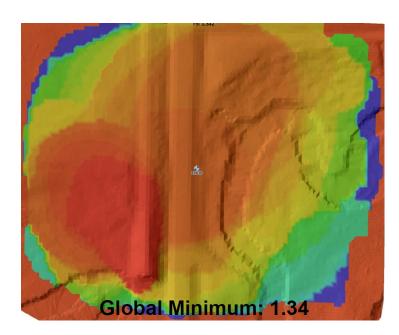


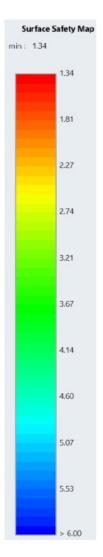


Number of points: 155,702,365

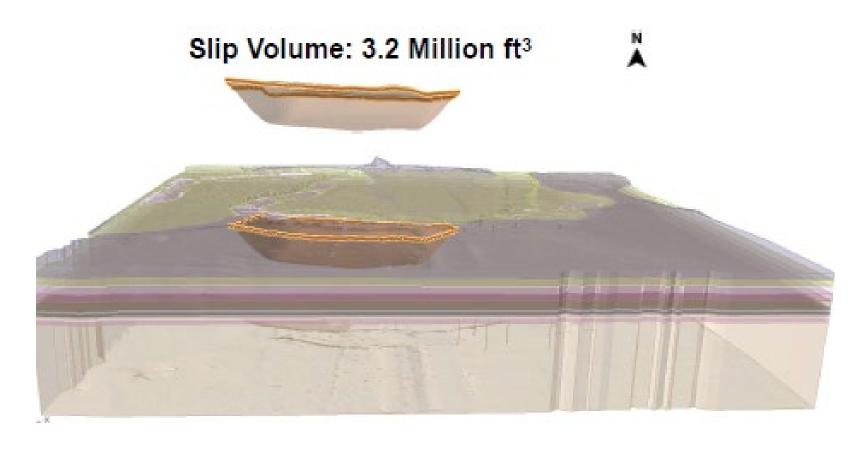
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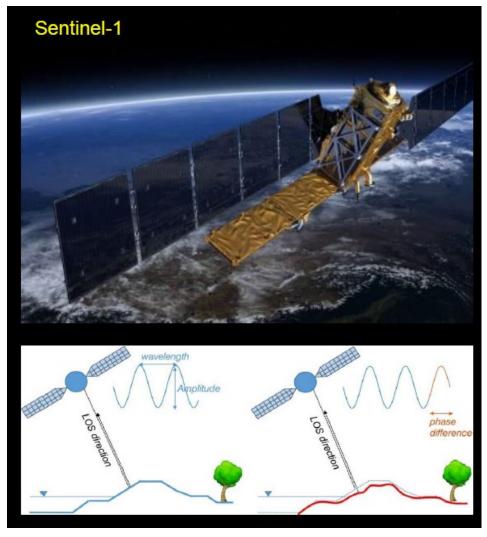


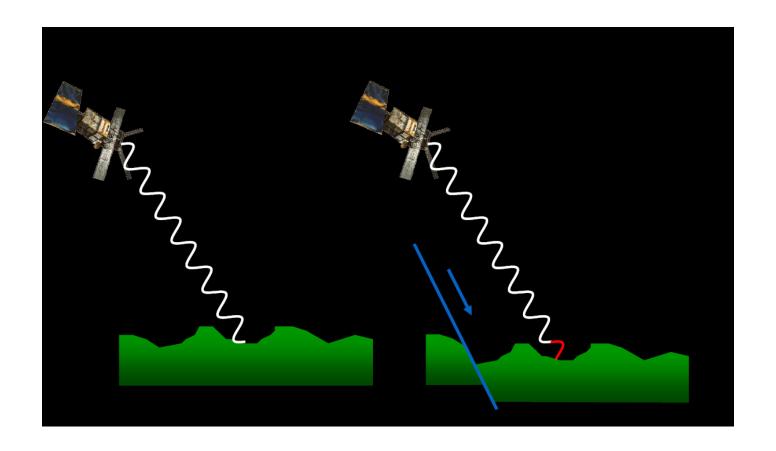


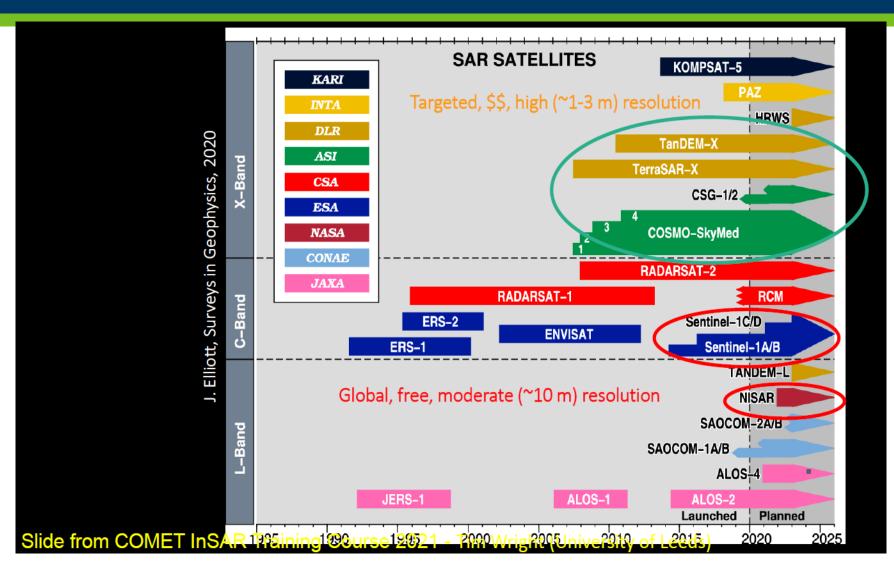


Climax, MN



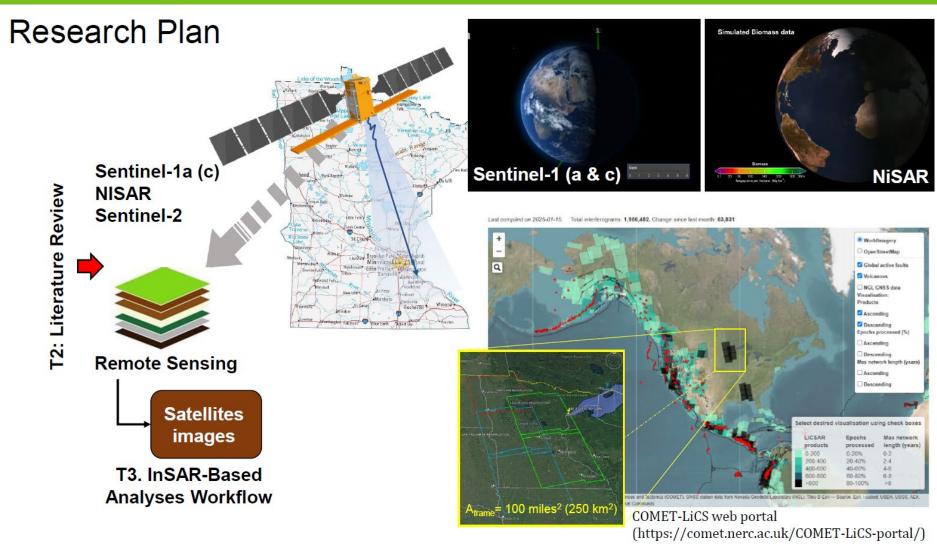


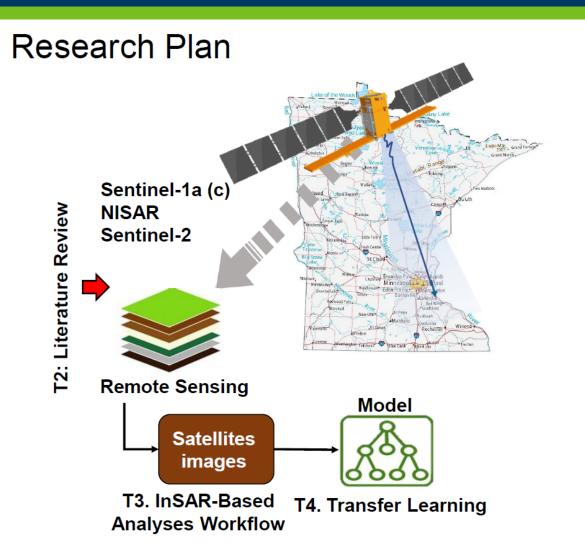


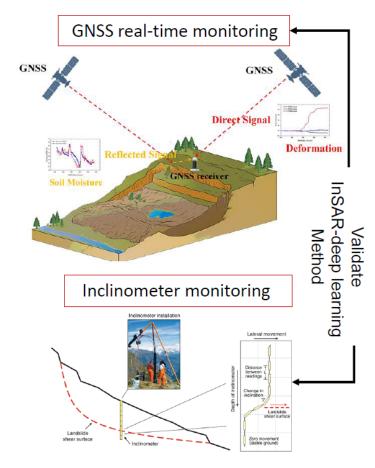


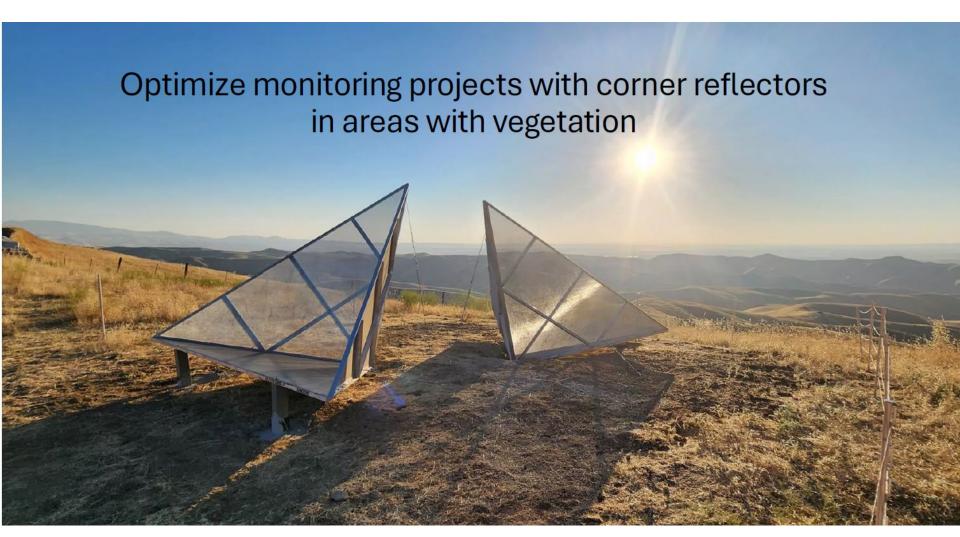
- Develop a fully automated, near real-time monitoring system to detect and extract abnormal ground deformation along highways using:
 - Interferometric Synthetic Aperture Radar (InSAR)
 - SAR
 - Optic data
 - Combined with in-situ data (GNSS and corner reflectors)





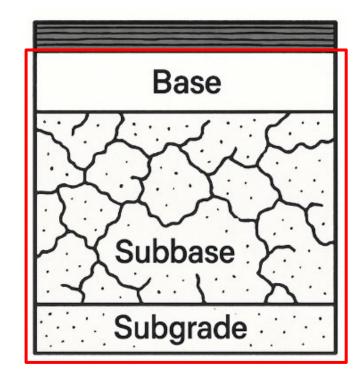


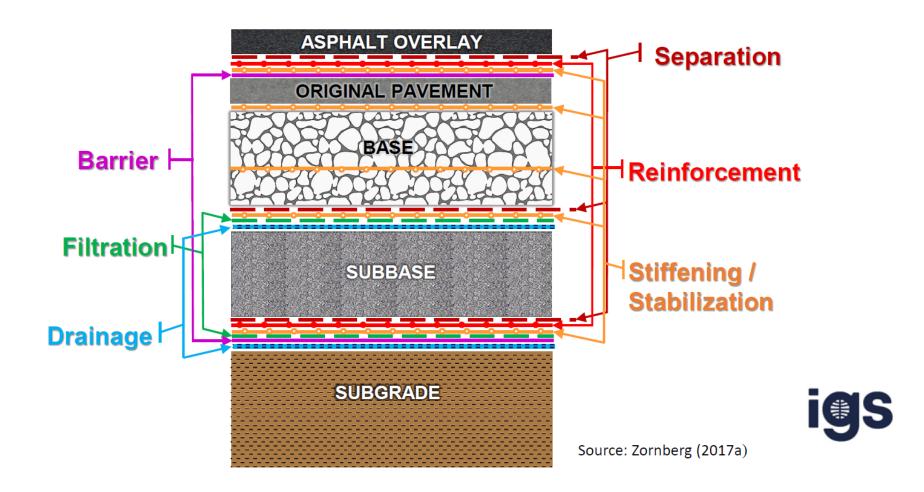




In the context of <u>Geosynthetics</u> in Pavement Foundations:

- Improve/update general guidelines and specs
- Framework to add benefits of geosynthetics in:
 - Pavement design (MnPAVE)
 - LCCA





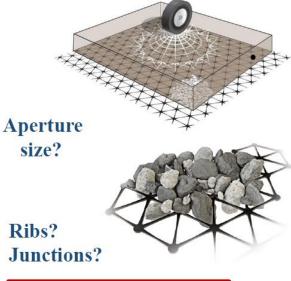
Geogrids vs Geotextiles for Stabilization

Geogrid

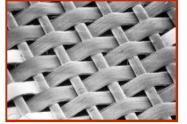
Geotextile

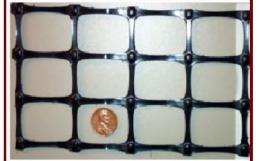














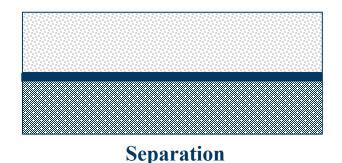
Woven



When to Use Geosynthetics?

- Deal with poor/soft subgrade
- Improve structural support of traffic loads
- Extend service life of pavement
- Reduce thickness of pavement foundation layers
- Increase reliability of design (e.g., reduce subgrade variability)
- To account for actual subgrade stiffness/strength lower than assumed stiffness/strength in design
- Improve water management in pavement system

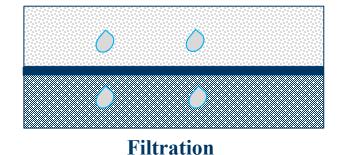
Mechanisms



Properties for Consideration:

- Soil/Aggregate:
 - Relatively high contrast in gradations for layers in contact (e.g., coarse subbase on fine subgrade)
- Geotextile:
 - Permittivity

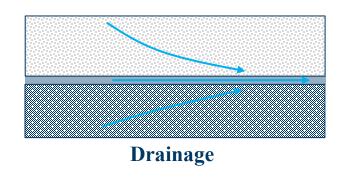
Mechanisms



Properties for Consideration:

- Soil/Aggregate:
 - N/A
- Geotextile:
 - Permittivity and Apparent Opening Size (AOS)

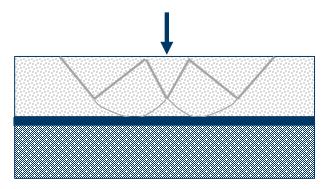
Mechanisms



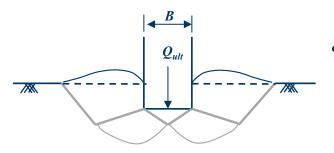
Properties for Consideration:

- Soil/Aggregate:
 - N/A
- Geotextile:
 - Permittivity and Apparent Opening Size (AOS)
- Pavement Geometry:
 - x-slope

Mechanisms



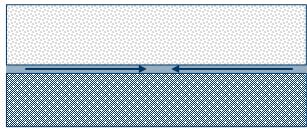
Reinforcement



Properties for Consideration:

- Soil/Aggregate:
 - Gradation and Particle Shape
- Geotextile:
 - Apparent Opening Size (AOS) and Tensile Strength
- Geogrid:
 - Grid Aperture Size and Tensile Strength

Mechanisms



Confinement (lateral restraint)

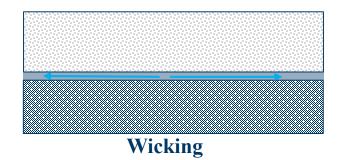
Properties for Consideration:

- Soil/Aggregate:
 - Gradation and Particle Shape
- Geotextile:
 - Apparent Opening Size (AOS)
- Geogrid:
 - Grid Aperture Size
 - Size geogrid according to

 $D_{50} \le \underline{\text{Geogrid Aperture Size}} \le 2*D_{85}$

Note: Use the smaller grid aperture dimension

Mechanisms

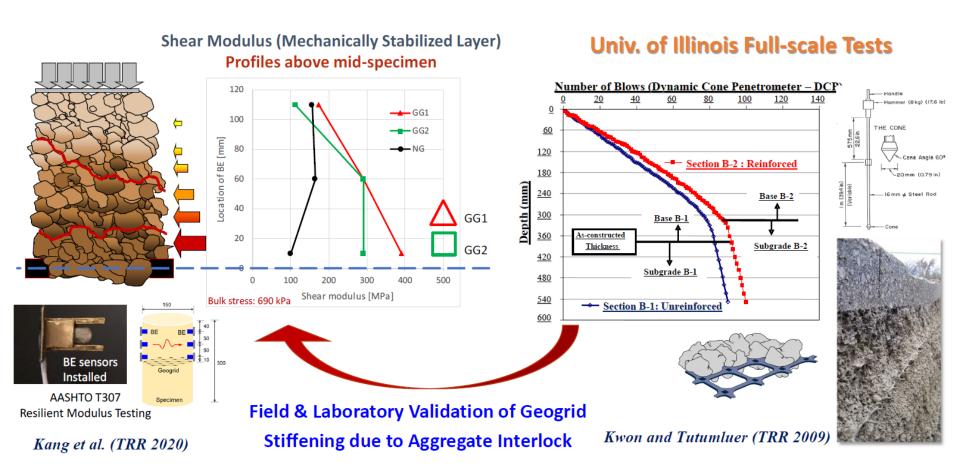


Properties for Consideration:

- Soil/Aggregate:
 - Classification
- Geotextile:
 - Permittivity, AOS, Flow Rate, Wet Front Movement
- Pavement Features:
 - Proper Drainage System(e.g., ditch, edge drains, etc)

MnDOT Geotextile Guideline

Soil Type/Rvalue/DCP/CBR	R _{value}	DCP	CBR	MnDOT Type	Separation	Filtration	Drainage	Reinforcement	Confinement	Moisture Management	Approx. Cost
Good to marginal dry soils	>25	<20	>6	4	Yes	Yes	Yes	Yes	No	No	\$
Good to marginal dry soils	>25	<20	>6	7	Yes	Yes	Yes	Yes	No	No	\$
Weak Dry/Damp Soils	15-25	20- 60	3-6	New 5	Yes	Yes	Yes	Yes	Yes	No	\$
Weak Dry/Damp Soils	15-25	20- 60	3-6	9	Yes	Yes	Yes	Yes	Yes	No	1.5 x \$
Weaker Damp Soils	<15	>60	<3	10	Yes	Yes	Yes	Yes	Yes	No	1.5 x \$
Very weak and/or wet soils	<15	>60	<3	11	Yes	Yes	Yes	Yes	Yes	Some Manufactures	2 x \$
Very weak and/or wet soils	<15	>60	<3	12	Yes	Yes	Yes	Yes	Yes	Some Manufactures	2 x \$
Very weak and/or wet soils	<15	>60	<3	13	Yes	Yes	Yes	Yes	Yes	Yes	2 x \$



RCA Main Environmental and Performance Issues

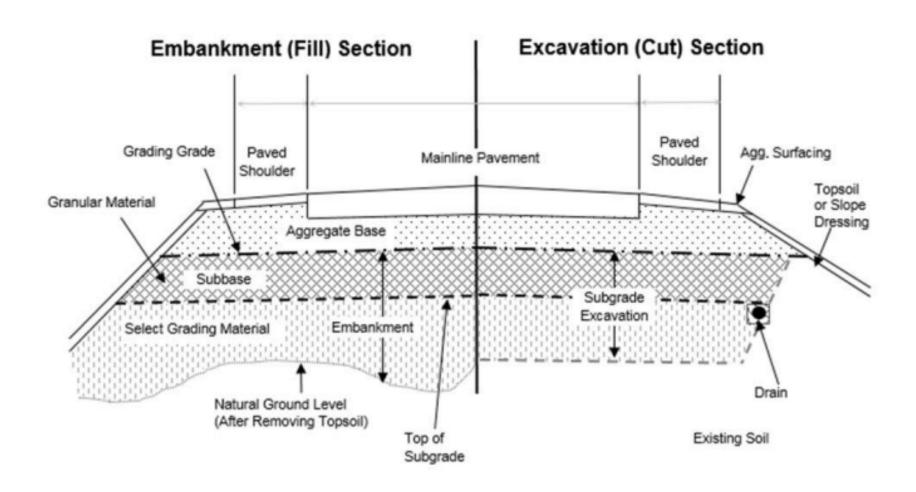
- Environmental:
 - High pH
 - Leaching of heavy metals
- Performance (drainage):
 - Tufa formation (calcium carbonate)





Photos: PennDOT

Where to use RCA?



RCA in Pavement Foundations

LOCATION OF TEST CELLS

- 4 x Test Cells
 - Cell 185 Coarse RCA
 - Cell 186 Fine RCA
 - Cell 188 Limestone (Virgin Aggregate)
 - Cell 189 RCA+RAP

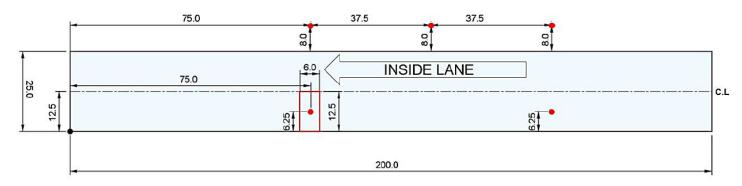


CELL 185	CELL 186	CELL 188	CELL 189
3.5in Asphalt	3.5in Asphalt	3.5in Asphalt	3.5in Asphalt
12in Coarse RCA	12in Fine RCA	12in Limestone (VA)	12in RCA + RAP
3.5in Sand Subbase	3.5in Sand Subbase	3.5in Sand Subbase	3.5in Sand Subbase
Sand	Sand	Clay Loam	Clay Loam



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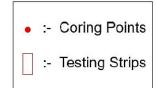
Sample Collection



^{*}All measurements are in feet.

2 x Sampling points on the section (with 3 on shoulders)

1 x Test Strip



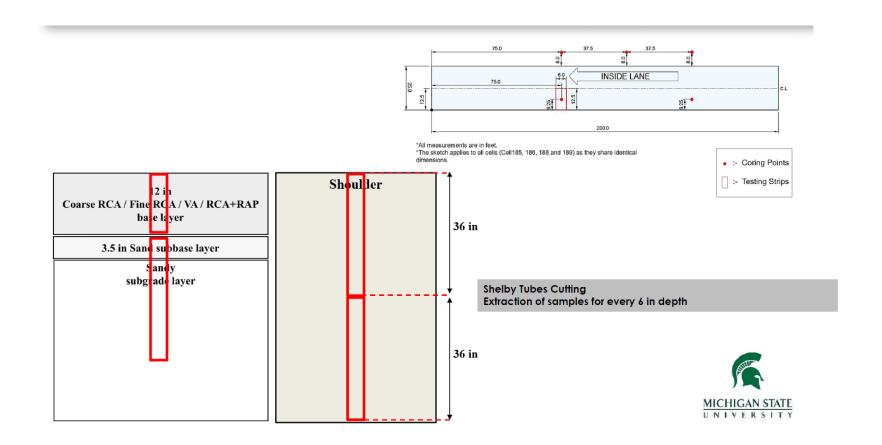
ORDER OF WORK PRIORITY

FINE RCA (Cell 186) > LIMESTONE (Cell 188) > COARSE RCA (Cell 185) > RCA+RAP (Cell 189)

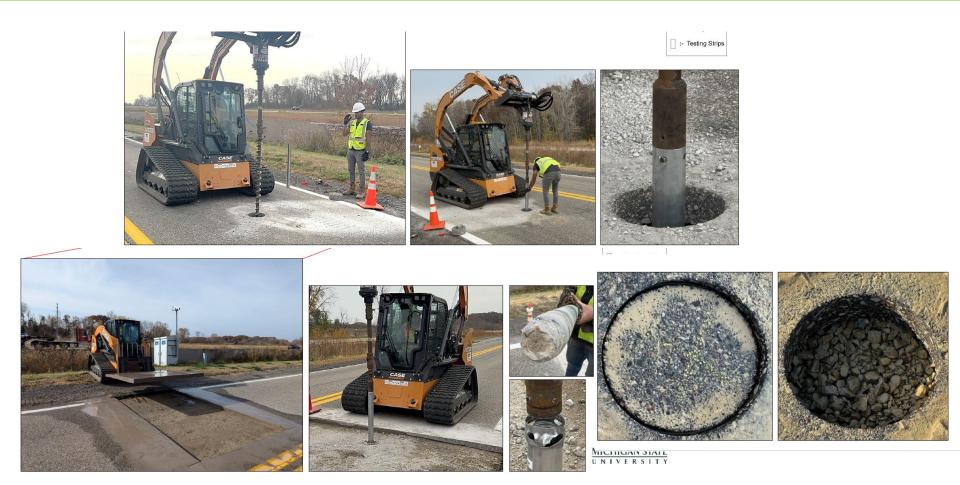


^{*}The sketch applies to all cells (Cell185, 186, 188 and 189) as they share identical dimensions.

Sample Collection (cont)



Field Work



Leaching Tests

Parameters	Details
Particle Size (85% wt less than)	No 4 sieve
Minimum Dry Mass (g-dry)	80 ± 0.02
Contact Time (hours)	72 ± 2
Effluent (DI Water) Concentration	1000 ml
Vessel Size	2000 ml
Revolutions (rpm) for EPA 1316	28 ± 2



AIR DRYING OF SAMPLES

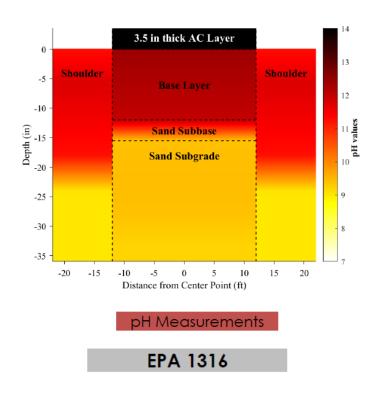


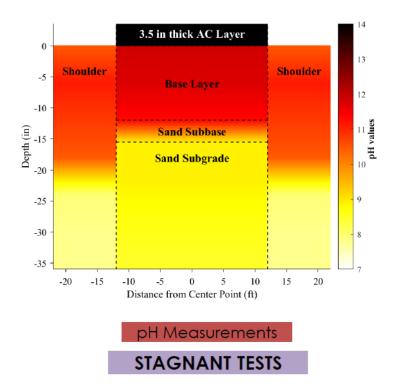
LEACHING TEST (EPA 1316)



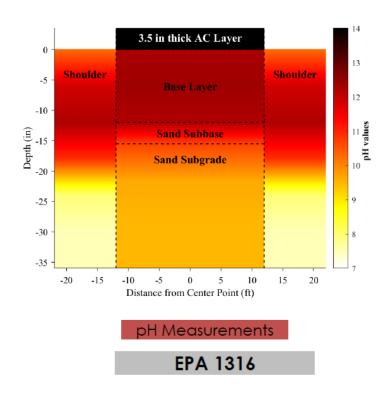
LEACHING TEST (STAGNANT PROCEDURE)

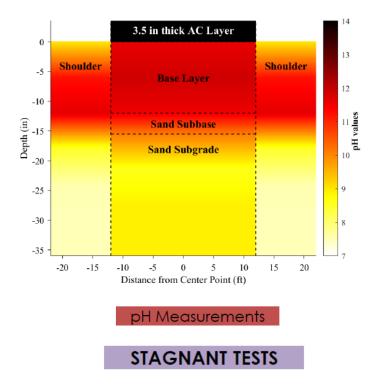
Test Results (Cell 185 Coarse RCA)



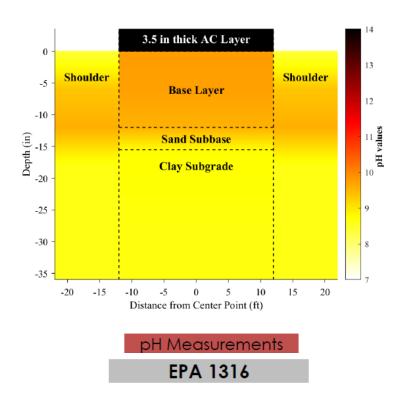


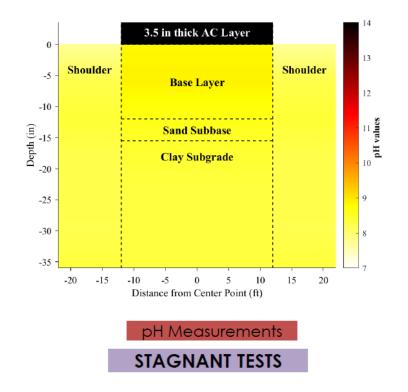
Test Results (Cell 186 Fine RCA)



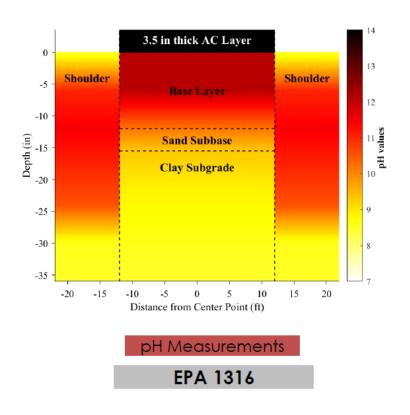


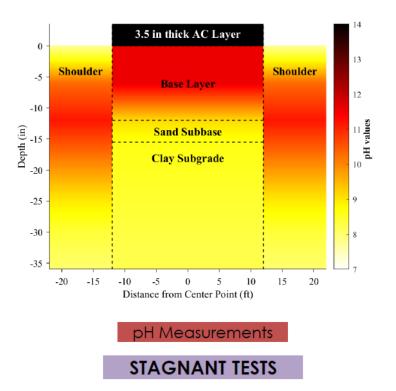
Test Results (Cell 188 Limestone)





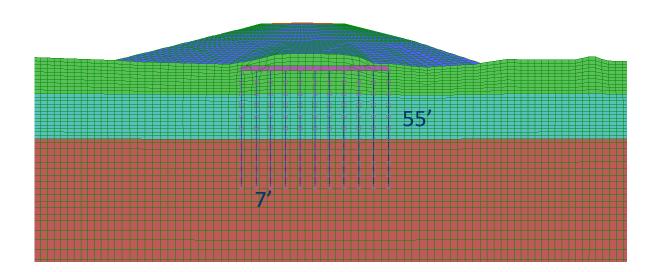
Test Results (Cell 189 RCA+RAP)



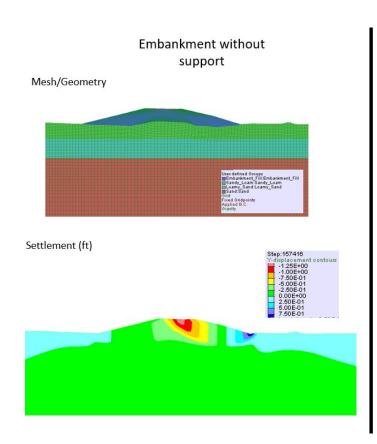


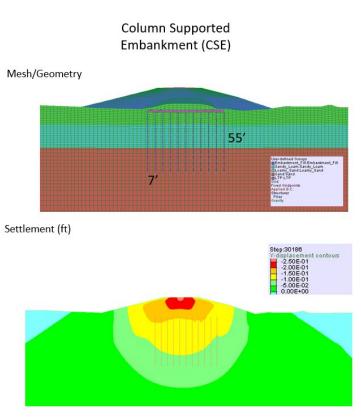
Optimization of CSE

 Implementation of Advanced Geotech Modeling Software for Complex Projects

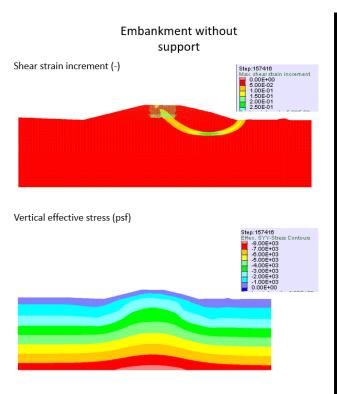


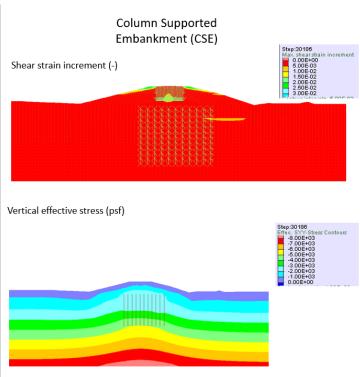
TH-93 – Column Supported Embankment (CSE)



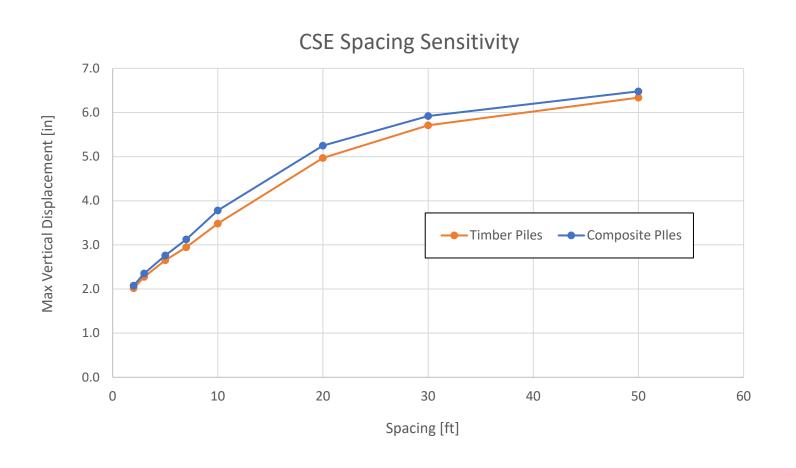


TH-93 – Column Supported Embankment (CSE)





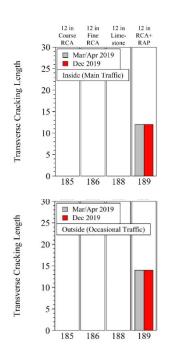
TH-93 – Column Supported Embankment (CSE)

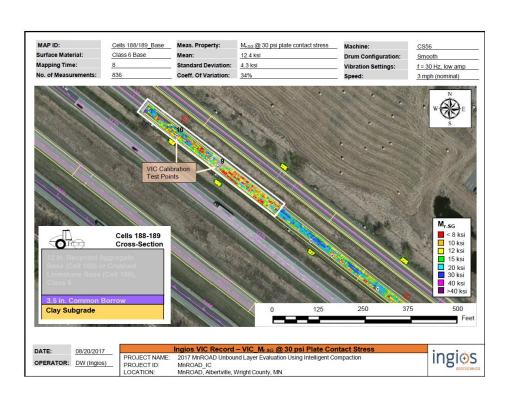


Pavement Foundation Uniformity (aka IC)



Pavement Foundation Uniformity





White and Vennapusa (2017)

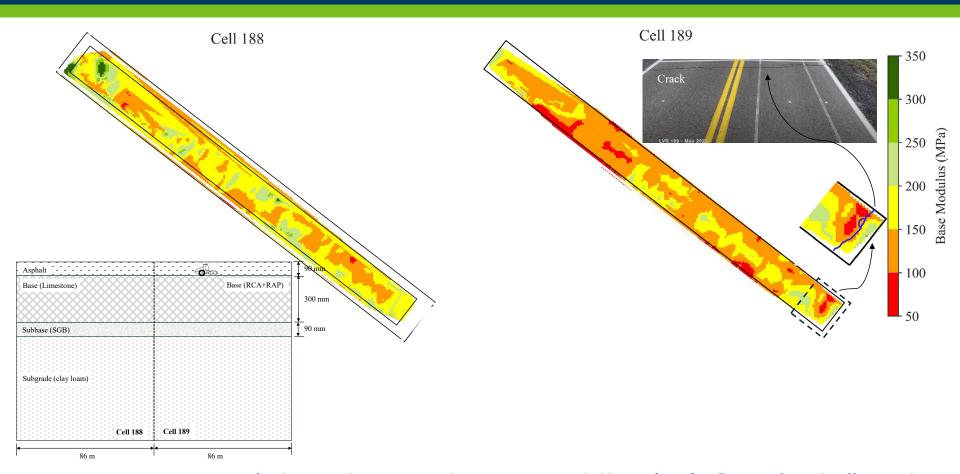
Pavement Foundation Uniformity





*Sadiq, M., Velasquez, R., Aydin, C., Cetin, B., Izevbekhai, B. (2025), Influence of Initial Stiffness and Foundation Uniformity on Pavement Performance, IJPE

Pavement Foundation Uniformity

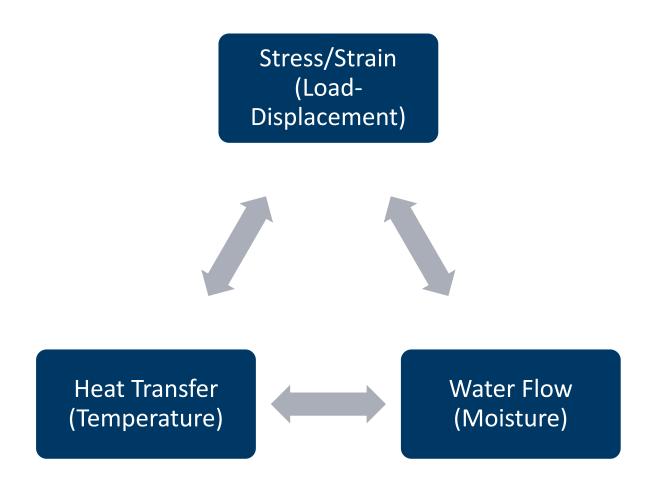


*Sadiq, M., Velasquez, R., Aydin, C., Cetin, B., Izevbekhai, B. (2025), Influence of Initial Stiffness and Foundation Uniformity on Pavement Performance, IJPE



~15,000+ Sensors Installed

Temperature
~ 1 billion total
values





Processing Data with Descriptive Statistics:

Mean

Max

Min

Median

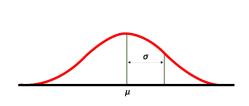
Variance

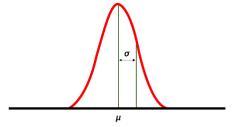
Standard Deviation

Kurtosis

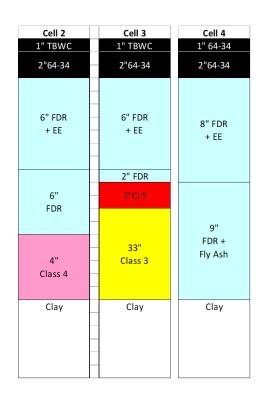
Skewness

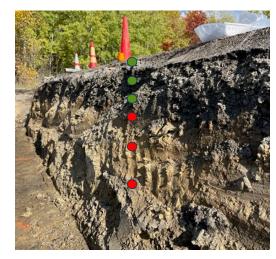
Range

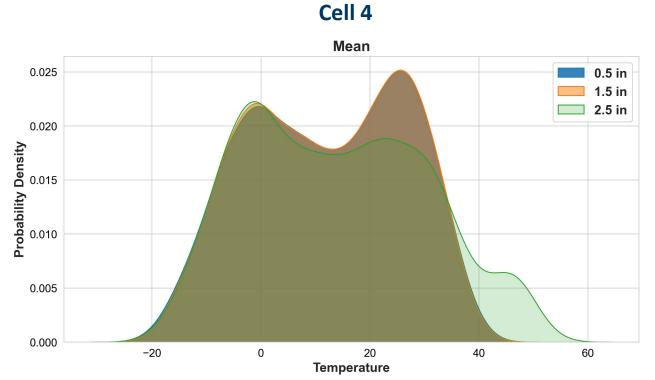


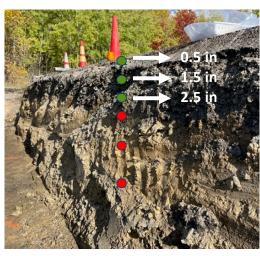


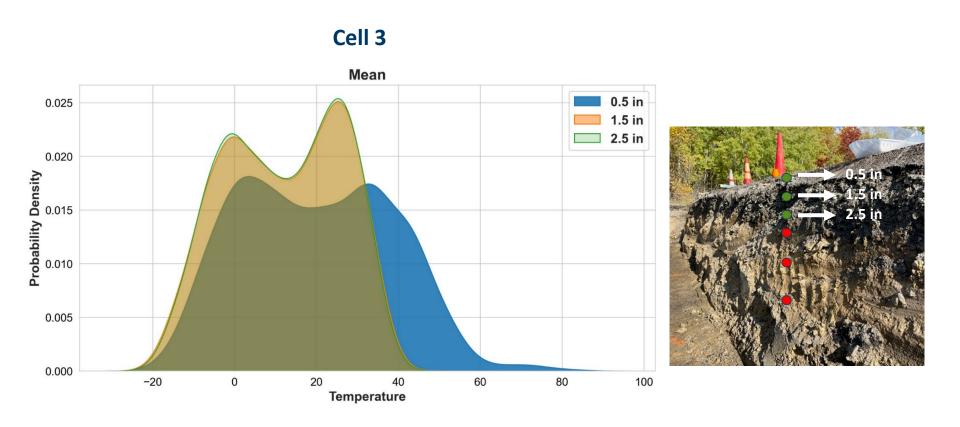
- Collected data from 3 flexible pavement test sections
 - Built on different foundations such as aggregate, Full Depth Reclamation (FDR) and Stabilized Full Depth Reclamation (SFDR)
 - Test section 2 and 3 have proper drainage vs Test section 4 that is directly on top of clay layer

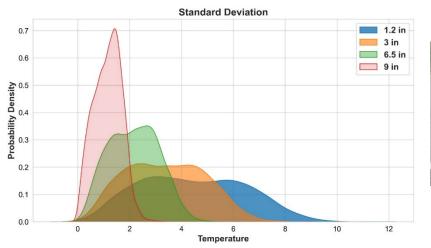




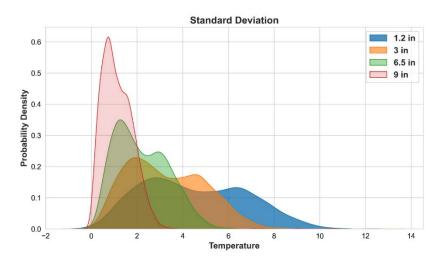






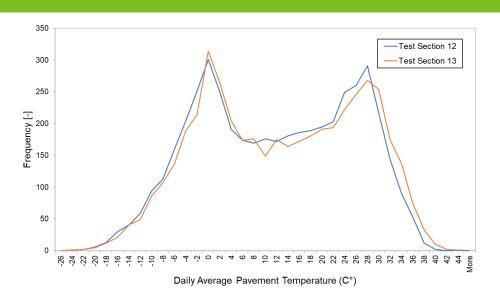


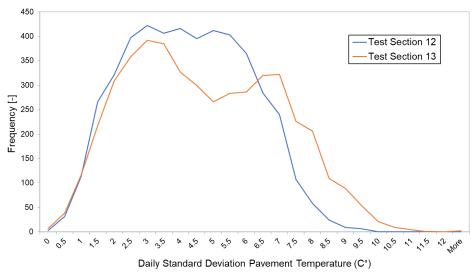






12	13	_	
10" PCC	10" PCC	##	1.2 in 3.0 in 6.5 in 9.0 in
5" Class 5	5" Class 5		
Special	Special		
Clay	Clay		
Panel Size	Panel Size		
Panel Size 15x12	Panel Size 20x12		
15x12	20x12		
15x12 dowel	20x12 dowel		
15x12 dowel	20x12 dowel		

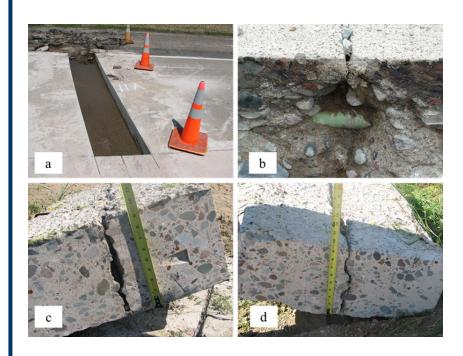




Good Pavement - Test Section 12



Distressed Pavement – Test Section 13



THANK YOU!

2025 Midwest Geotechnical Conference

September 23-25, 2025 Sheraton City Centre Hotel, Indianapolis, Indiana



